

Consideration of cathode specific surface area and hydrodynamics in scaling up microbial fuel cells

Bruce E. Logan
Penn State University





What do we need to commercialize MFCs?

- Now have >1 decade of MFC research... why don't we have commercialized MFCs?
- Bacteria: Geobacter sp
- Materials: both electrodes < \$100 m⁻²
 - Anode: many choices; brushes still superior
 - Cathode: activated carbon(s)
- Architecture: Tubular vs plate/frame?
- Manufacturing: Cathode production?
- Secondary processes needed!



What microbes are on the anodes?

- Tested reactors over 2 months from 3 sources
 - Penn State wastewater treatment plant (P)
 - UAJA wastewater treatment plant (U)
 - Freshwater bog sediments (B)
- Performance analysis: Power production
- Community analysis
 - Clone libraries
 - Pyrosequencing
 - DGGE
 - FISH

Wastewater Treatment plants:

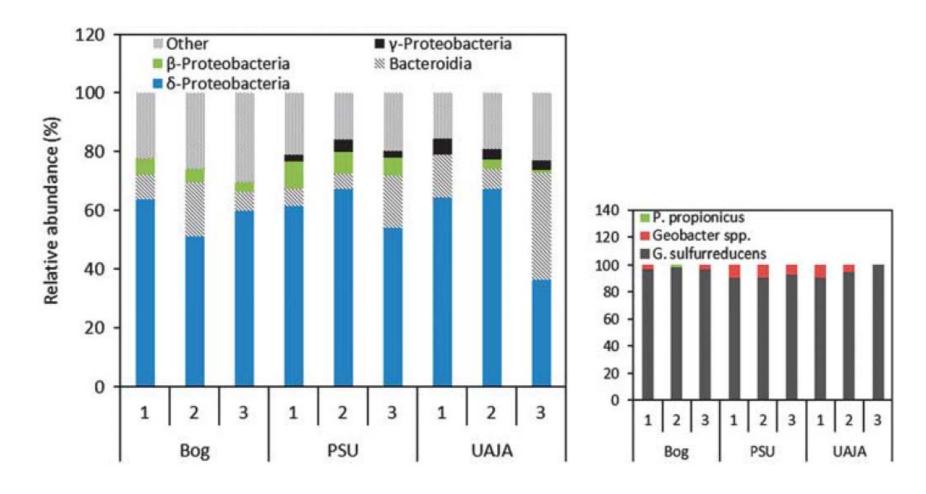
P=PSU, U=UAJA





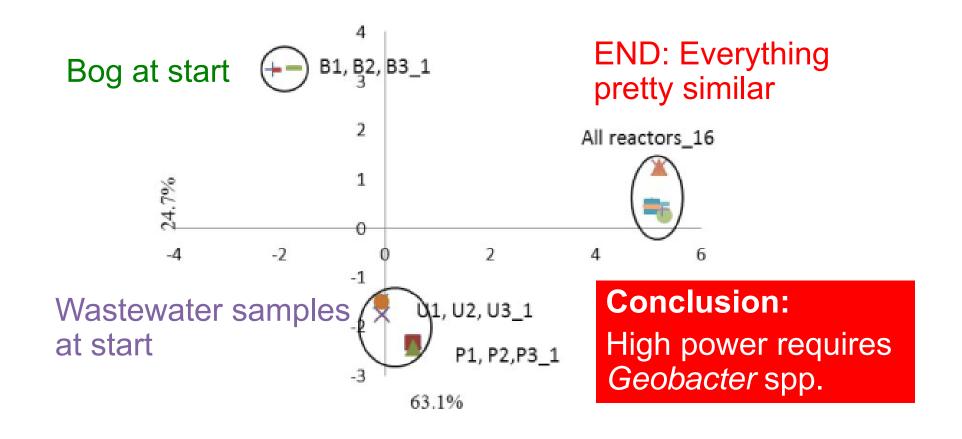


<u>Pyrosequencing:</u> mostly Delta Proteobacteria... and of those, almost all sequences most similar to *Geobacter sulfurreducens*





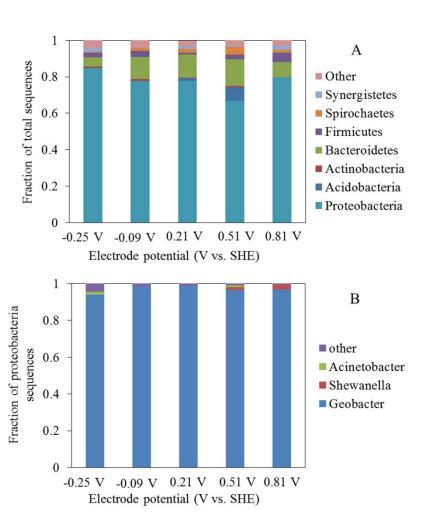
DGGE used to show changes in community diversity over time



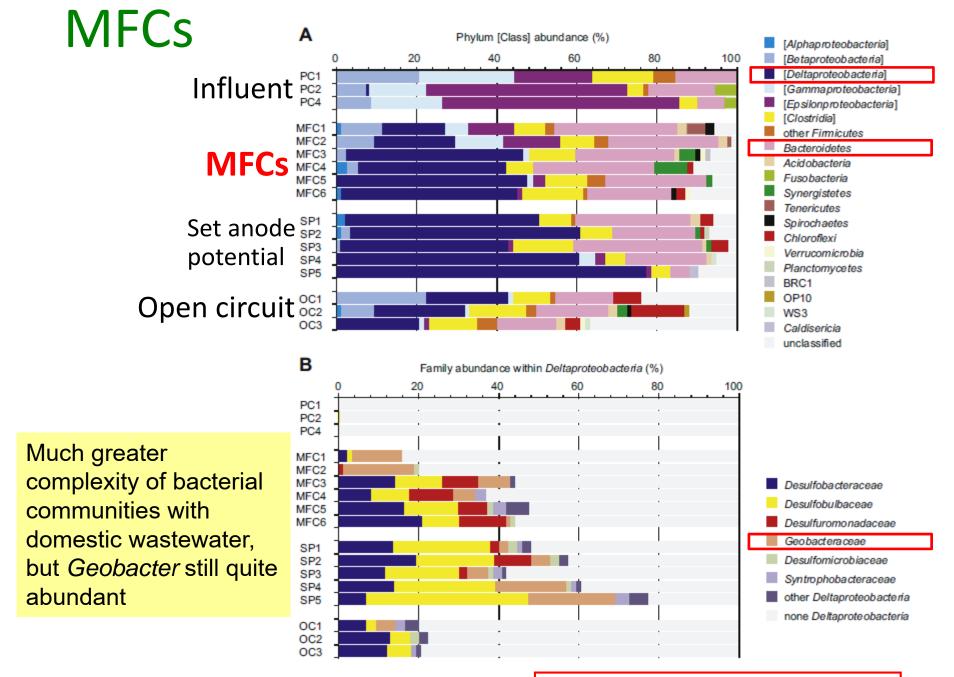


Community composition unchanged at varied set potentials when different reactors used

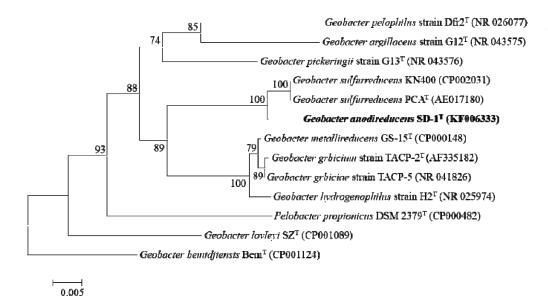






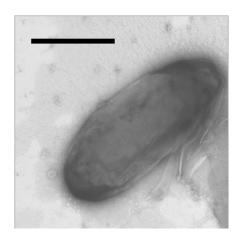


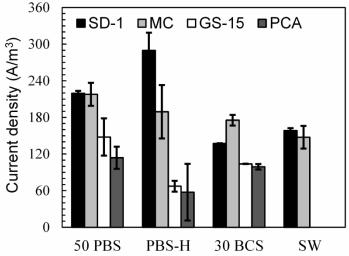
Isolate from MFC: Geobacter anodireducens SD-1



Characteristics of *G. anodireducens* SD-1 (*Geobacter sulfurreducens* PCA)

- Isolated from MFC fed formate, 98% similarity to strain PCA
- DNA-DNA hybridizations show a relatedness of 61.6% with PCA (<70%)
- Tolerates up to 3% NaCl (vs 1.7% for PCA)
- Grows well in 200 mM phosphate buffer (PCA does not grow)
- Cannot grow using fumarate as electron acceptor (PCA can grow)





50 PBS: 50 mM phosphate buffer

PBS-H: 200 mM PBS

30 BCS: 30 mM bicarbonate buffer SW: 3% NaCl (like seawater)

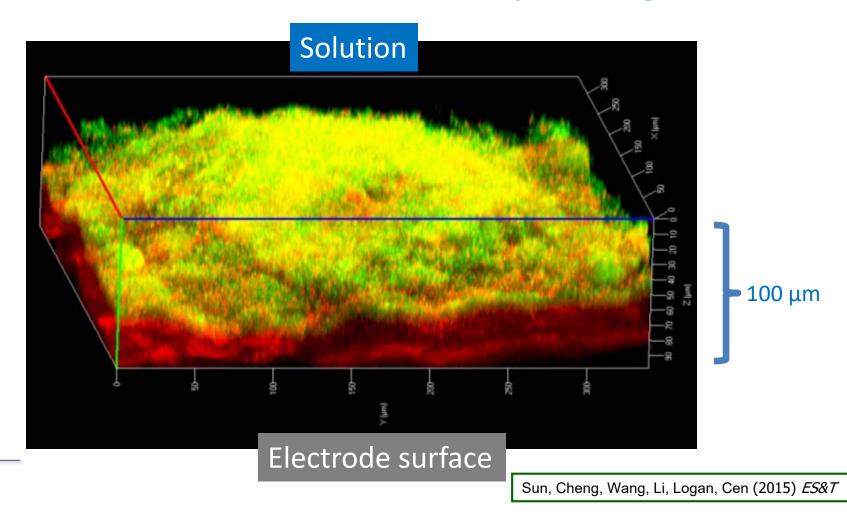


Sun, Wang, Cheng, Yates, Logan (2014) *Int. J. System. Evol. Microbiol.*

Electrogenic Biofilms

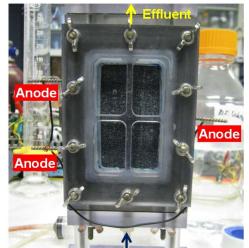
 Dead biofilm (red) remains electrically conductive for active biofilm (yellow/green)

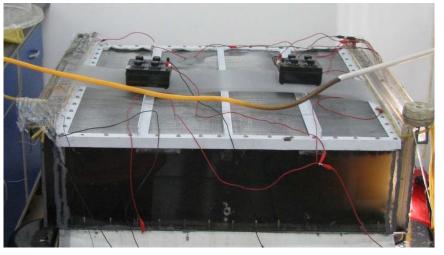
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Scaling up MFCs











MFC Architecture

CHEMSUSCHEM



DOI: 10.1002/cssc.201100732

Bioelectrochemical Systems: An Outlook for Practical Applications

Tom H. J. A. Sleutels, [a] Annemiek Ter Heijne, $*^{[b]}$ Cees J. N. Buisman, [a, b] and Hubertus V. M. Hamelers [a, b]

Bioelectrochemical systems (BESs) hold great promise for sustainable production of energy and chemicals. This review addresses the factors that are essential for practical application of BESs. First, we compare benefits (value of products and cleaning of wastewater) with costs (capital and operational costs). Based on this, we analyze the maximum internal resistance (in $m\Omega m^2$) and current density that is required to make microbial fuel cells (MFCs) and hydrogen-producing microbial electrolysis cells (MECs) cost effective. We compare these maximum resis-

tances to reported internal resistances and current densities with special focus on cathodic resistances. Whereas the current densities of MFCs still need to be increased considerably (i.e., internal resistance needs to be decreased), MECs are closer to application as their current densities can be increased by increasing the applied voltage. For MFCs, the production of high-value products in combination with electricity production and wastewater treatment is a promising route.

Review



Towards practical implementation of bioelectrochemical wastewater treatment

René A. Rozendal^{1,2,3}, Hubertus V.M. Hamelers², Korneel Rabaey¹, Jurg Keller¹ and Cees J.N. Buisman^{2,3}

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Estimates for MFCs

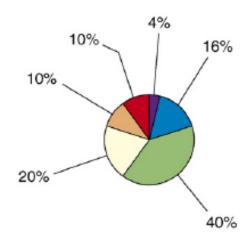
• 100 € /m² or \$130/m²

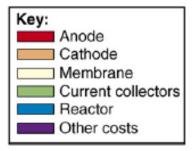
Estimates for MECs

• 100 € /m² or \$130/m²

(b) Future

(~0.4 €/kg COD)





¹ Advanced Water Management Centre, The University of Queensland, St. Lucia, QLD 4072, Australia

² Sub-department of Environmental Technology, Wageningen University, Bomenweg 2, P.O. Box 8129, 6700 EV Wageningen, The Netherlands

³ Wetsus, Centre for Sustainable Water Technology, Agora 1, P.O. Box 1113, 8900 CC Leeuwarden, The Netherlands

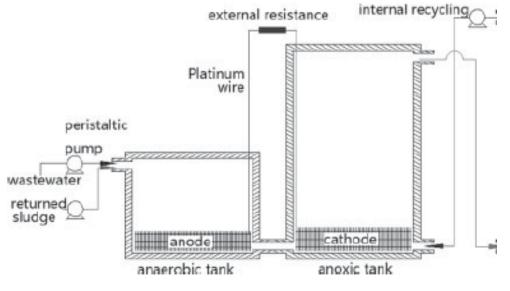
Design

- These are bad designs for treatment....Keep the electrodes close (but not too close!)
- You cannot design separate anode and cathode reactors!





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Xie et al. (2013) J. Chem. Technol. Biotechnol.

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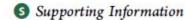
Review

pubs.acs.org/journal/estlcu

Assessment of Microbial Fuel Cell Configurations and Power Densities

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Science & Technology | + | | + | |



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To Design your MFC:

Materials

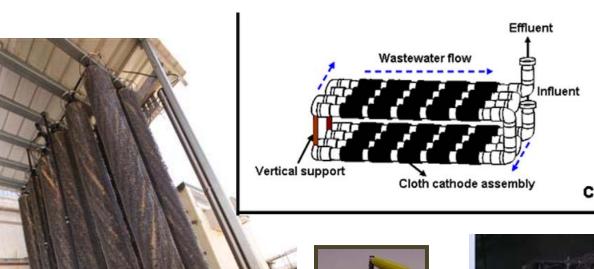
- Anode: Flat (cloth, felt, etc.), brush, granules, or other?
- Separator: fibrous or ion exchange membrane?
- Cathode: Activated carbon + binder + diffusion layer

Architecture:

- Plate/frame or tubular?
- Cathode specific surface area: A_{cat} (m²/m³)
 - Defined as cathode area per volume
 - Maximize A_{cat} based on MFC configuration



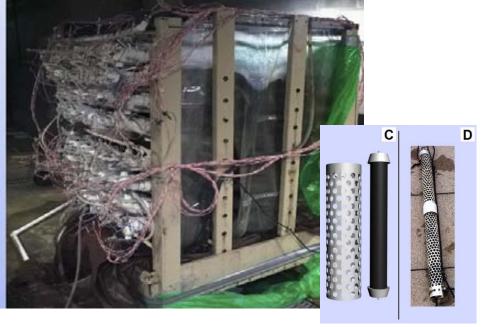
Tubular MFCs













Tubular/Cylindrical Designs

- A_{cat} (m²/m³) based on a cylinder diameter, d
 - Area of the cathode is: A_{cvl}
 - Volume of the MFC is: V_{cyl}

$$-A_{Cat} = \frac{A_{Cyl}}{V_{Cyl}} = \frac{\pi dL}{\frac{\pi}{4}d^2L} = \frac{4}{d}$$

- If d= 5 cm:
$$A_{Cat} = \frac{4}{d} = \frac{4}{(5 \text{ cm})} \frac{100 \text{ cm}}{m} = 80 \text{ m}^2/\text{m}^3$$

Tube designs need air flow around outside cylinder,
 so d = tube diameter + air space

- If
$$d = 5 cm + 2 cm$$
, $A_{Cat} = 57 \text{ m}^2/\text{m}^3$



The Largest Tubular MFC



- $A_{cat} = 22 \text{ m}^2/\text{m}^3 \text{ based } d = 18 \text{ cm}$ (volume around tubes not included)
- Performance not published in peer reviewed literature, but:
 - Tested brewery wastewater
 - Produced 330 mW/m² (8 W/m²)
 - HRT= unknown



Small tube MFC

- Two tubes, each 2 L in volume (4 L total)
- $A_{cat} = 80 \text{ m}^2/\text{m}^3 (d=5 \text{ cm, just the tube; each } 100 \text{ cm long})$
- HRT = 11 h
- Power = $10-50 \text{ mW/m}^2$
- Final COD= 80–100 mg/L
- CE=11%





Racks of many smaller tube MFCs

- 200 L based on 96 tubes, each ~2 L in volume
- $A_{cat} = 80 \text{ m}^2/\text{m}^3 (d=5 \text{ cm, just the tube; each } 100 \text{ cm long})$
- 6 9 mW/m² (84 130 mW, 15 m² cathode)
- HRT = 12 h
- Final COD= 33 mg/L

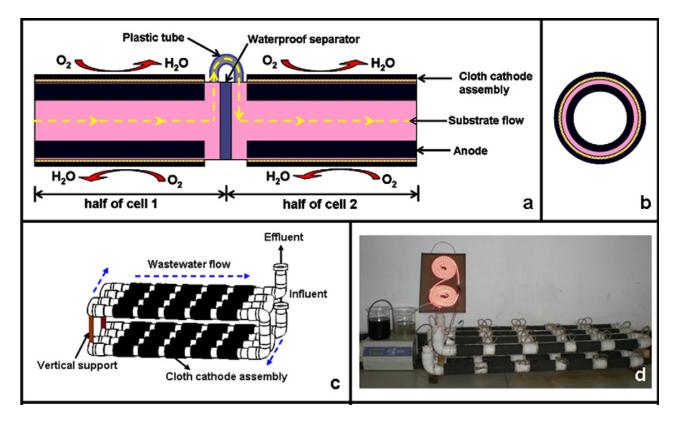




Ge et al. (2015) Energy extraction from a large-scale microbial fuel cell system treating municipal wastewater. *J. Power Sources.* 297:260-264 Personal communication: Prof. Zhen He

Serpentine MFC design

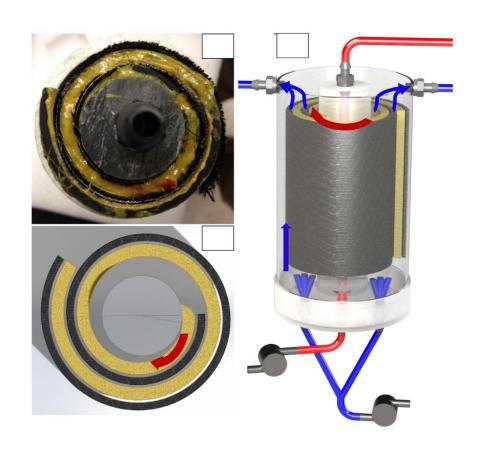
- $A_{cat} = 86 \text{ m}^2/\text{m}^3$ based estimated d=4.6; no volume around tubes
- $A_{cat} = 62 \text{ m}^2/\text{m}^3$ based on given summed electrode areas
- Produced 66 mW/m²; HRT= ???; connector tube could clog





Wound stack electrodes

- Cylinder, but more similar to a <u>plate</u> design: more of a "wound plate"
- Not ww or air:
 - Acetate
 - Percarbamate cathode (O₂ release compound)
- 2 Designs (HRT=20 min)
 - $-350 \text{ m}^2/\text{m}^3$; 94 mW/m²
 - $-700 \text{ m}^2/\text{m}^3$; 73 mW/m²





Plate/Frame MFCs



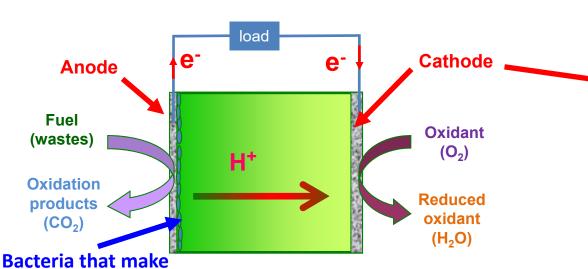






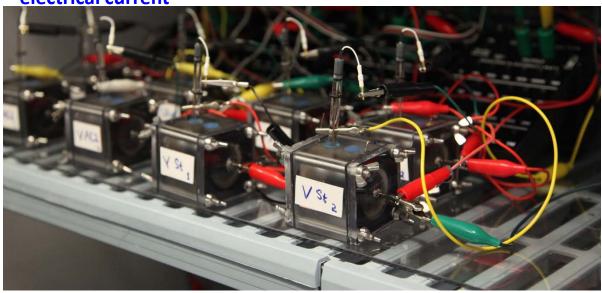


Electrical power generation in a **M**icrobial **Fuel C**ell (MFC) using exoelectrogenic microorganisms





Bacteria that make electrical current

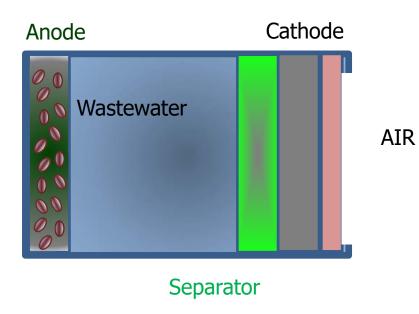




Liu et al. (2004) Environ. Sci. Technol.

MFC Materials





Low cost

\$/m² (US)

• Anode (brushes) \$20

Separator (cloth) \$ 1

Cathode \$15

- SS mesh

- AC + PVDF Binder

• TOTAL \$36



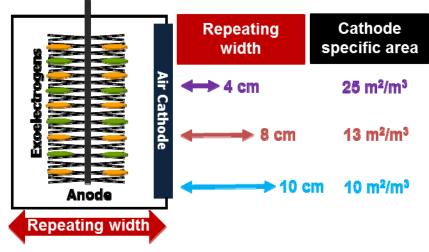
Key to cathode specific surface area is the "unit width"!

- Cathode specific surface area: A_{cat} (m²/m³)
 - Defined as cathode area per volume
 - Maximize based on MFC configuration
- Plate/Frame:
 - Width of anode chamber is: W_{An}
 - Width of cathode chamber is: W_{Cat}

$$-A_{Cat} = \frac{1}{W_{An} + W_{Cat}}$$

- If
$$W_{an} = 3 \text{ cm}$$
, $W_{Cat} = 1 \text{ cm}$
 $A_{cat} = 25 \text{ m}^2/\text{m}^3$







MFC Architecture



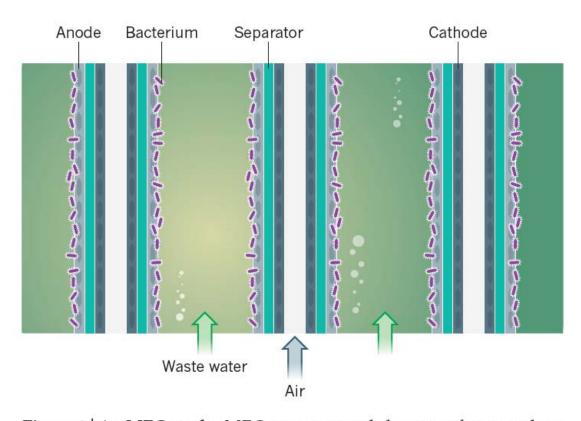
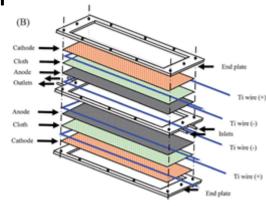


Figure 3 | An MFC stack. MFCs are arranged close together to reduce internal resistance and form compact reactors. Within the stack the electrodes consist of repeating units of an anode coated in a mat of bacteria, or biofilm, an insulating separator and a cathode. Waste water flows over the anodes and air over the cathodes. The individual anode and cathode are connected by a wire (not shown).



How close can electrodes be?

- Need room for electrodes, wastewater, air
- Acetate = no particles like real ww
- Too little space for ww→ clogging





 $25 \text{ m}^2/\text{m}^3$ (25 mL reactor)

Acetate: 2.8 W/m^2 (2.1 kW/m³)

WW: 0.5 W/m^2



 $680 \text{ m}^2/\text{m}^3$ (30 mL reactor)

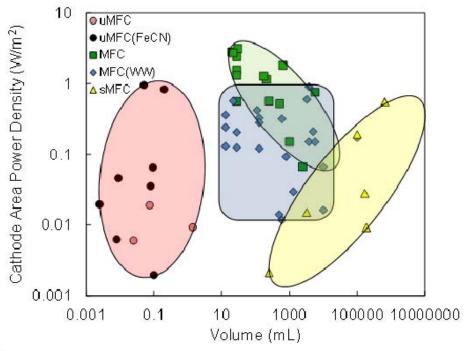
Acetate: $3.1 \text{ W/m}^2 (2.1 \text{ kW/m}^3)$

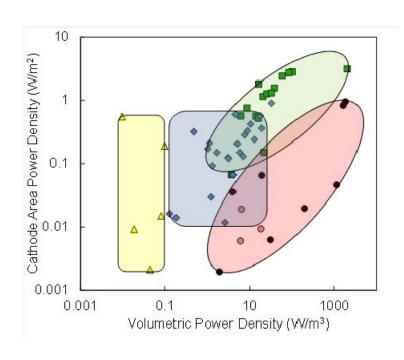
WW: (not tested)

Fan et al. (2013) Energy Env. Sci.

Range of power densities

- For MFCs treating single substrates area power density:
 - decreases with larger size reactors (left figure)
 - Shows an increase with volumetric density
- For MFCs treating wastewater, no trends!

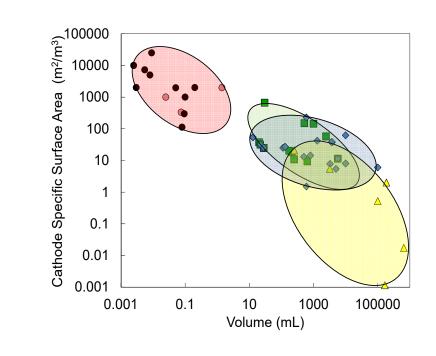


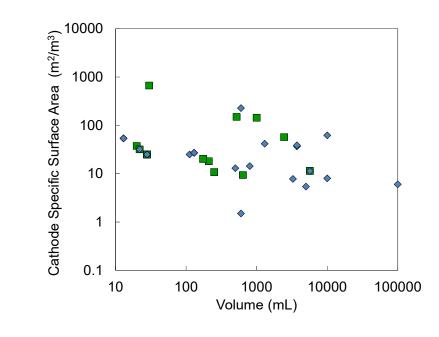






Cathode specific surface area decreases with reactor size







Electrode spacing?

- Flat electrodes: ≥ 2 cm
- Brush electrodes: Is closer is OK?

Environ. Sci. Technol. 2006, 40, 2426-2432

Increased Power Generation in a Continuous Flow MFC with Advective Flow through the Porous Anode and Reduced Electrode Spacing

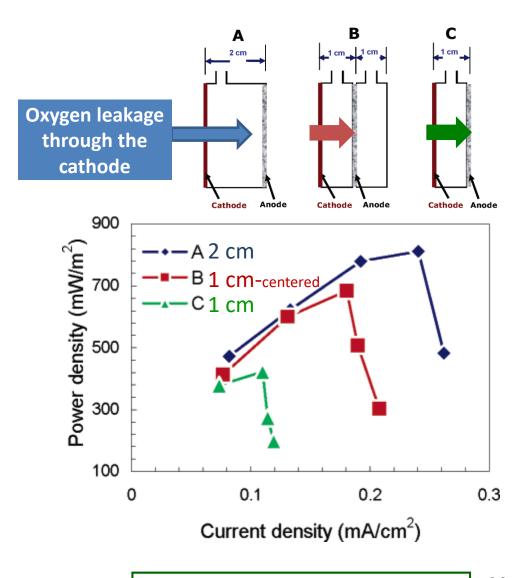
SHAOAN CHENG,† HONG LIU,† AND BRUCE E. LOGAN*,†,‡

Department of Civil and Environmental Engineering and The Penn State Hydrogen Energy (H₂E) Center, The Pennsylvania State University, University Park, Pennsylvania 16802

The maximum power generated in a single-chamber aircathode microbial fuel cell (MFC) has previously been shown to increase when the spacing between the electrodes is decreased from 4 to 2 cm. However, the maximum power from a MFC with glucose (500 mg/L) decreased from 811 mW/ m^2 ($R_{ex} = 200 \ \Omega$, Coulombic efficiency of CE = 28%) to 423 mW/ m^2 ($R_{ex} = 500 \ \Omega$, CE = 18%) when the electrode spacing was decreased from 2 to 1 cm (batch mode operation, power normalized by cathode projected area)

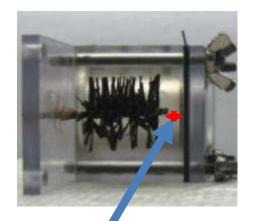
with both electrode One of the main wastewater treatmer generate electricity Power densities pro larger than those ob differences in powe tration and form (so kinetics, and the con the biofilm that is ne (9).

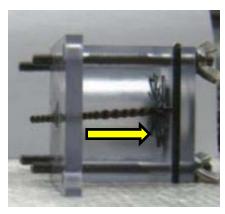
Power densities (modifying the and performance using produce high concer the PEM in systems et al. (14) achieved a mediator-producing However, ferricyani for wastewater treatr An advantage of us reaction is self-susta on cathodes, and al be reduced to as littl generation (16). Pr alternatives such as MPP) or iron(II) ph anly alightly radicas



Cheng, Liu, Logan (2006) Environ. Sci. Technol.

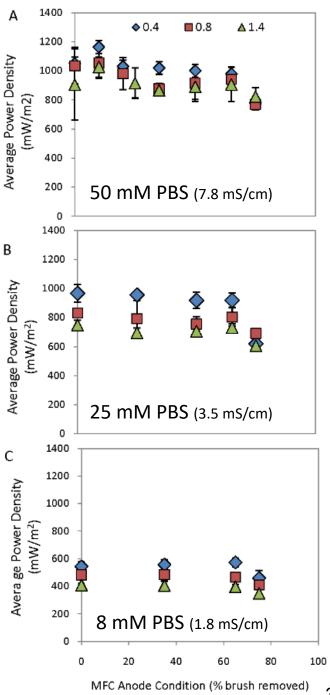
Brush to cathode distance





- Brush edge: 0.4, 0.8 or 1.4 cm
 - Closer brush works better, even up to 0.4 cm!
- 30-80% of brush removed from most distant side of the brush
 - No decrease in power until 80% of the brush removed. Brushes near the cathode are okay!

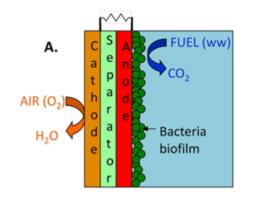


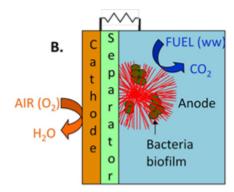


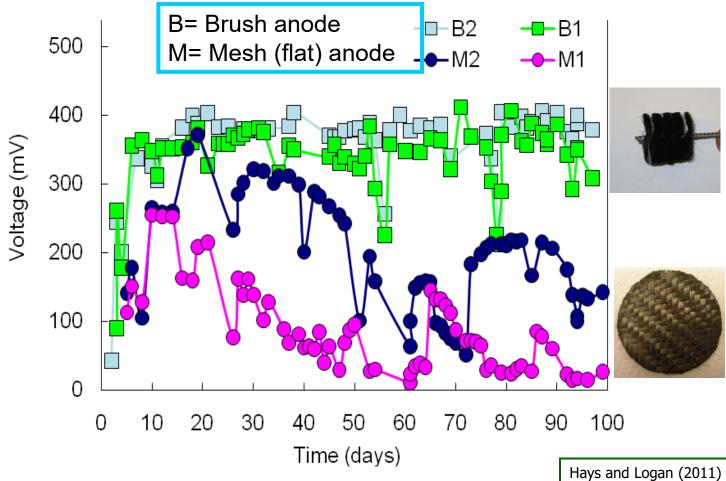
Voltage Production:

PENN!

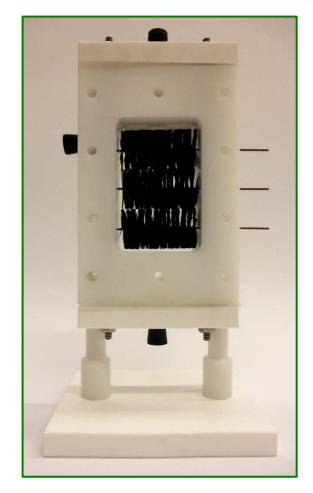
Mesh vs Brushes (domestic ww)



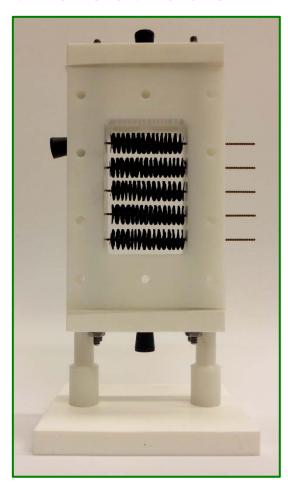




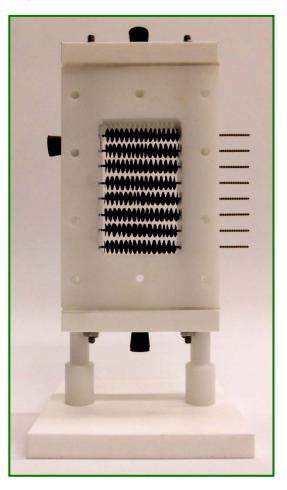
Multi-electrode MFCs



3 brushes (**R3**) 3500 m²/m³



5 brushes (**R5**) 2800 m²/m³



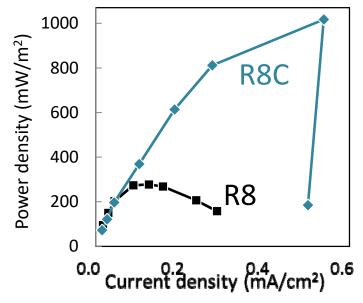
8 brushes (**R8**) 2900 m²/m³



Electrode area (2.5 cm diameter brush/chamber width = $40 \text{ m}^2/\text{m}^3$

Smaller, closer brushes work best.. with acetate

(Continuous flow, acetate in buffer)



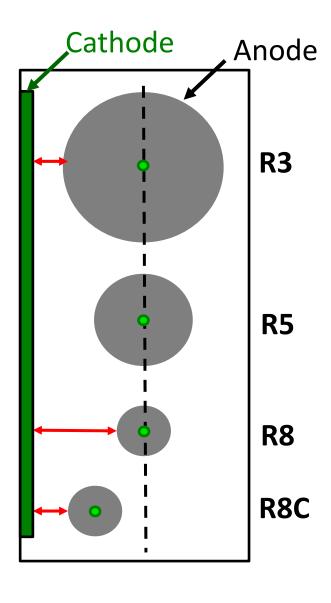


Maximum power densities

R8C= 1020 mW/m²

R8= 280 mW/m²

(R3= 560 mW/m^2) (not shown)

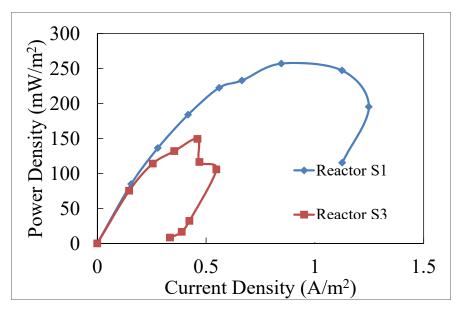




Lanas & Logan (2013) J. Power Sources

Reactor instability smaller brushes: wastewater

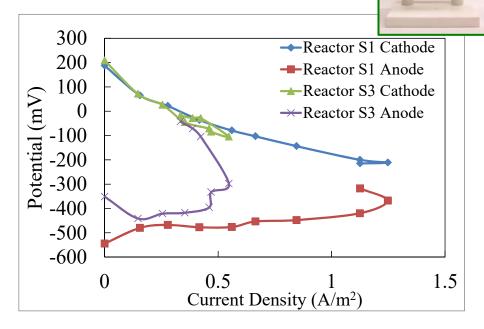
Continuous flow, 4 h HRT, domestic ww





260 mW/m² vs 150 mW/m²

Not possible to get true "duplicates"



- Cathode performance similar
- Anodes performance unstable (S3)

Conclusion: Avoid the use of very thin brushes (it produces conditions similar to "flat anodes")

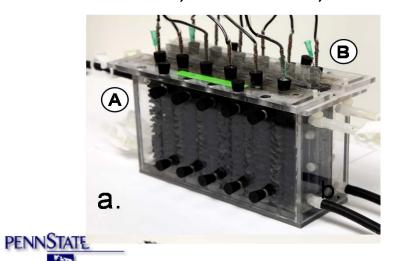


Reactor Designs

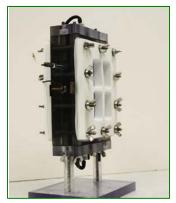
Gen 0: 0.025 L, 25 m²/m³



Gen 2: 2 L, 2 chambers, 25 m²/m³

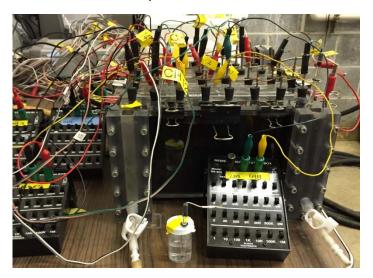


Gen 1: ~0.13 L, 25 m²/m³





Gen 3: 5.7 L, 4 chambers

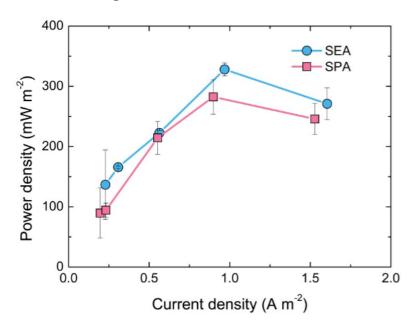


Gen 1 MFCs: Separator or no separator?



Separator No-separator (Separator Electrode (Spaced electrode Assembly, SEA) assembly, SPA) SEA SPA Separator Cathode 0.8 cm Anode 0.5 cn 2.0 cm

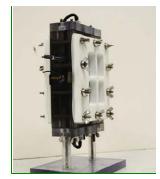
Tests using domestic wastewater

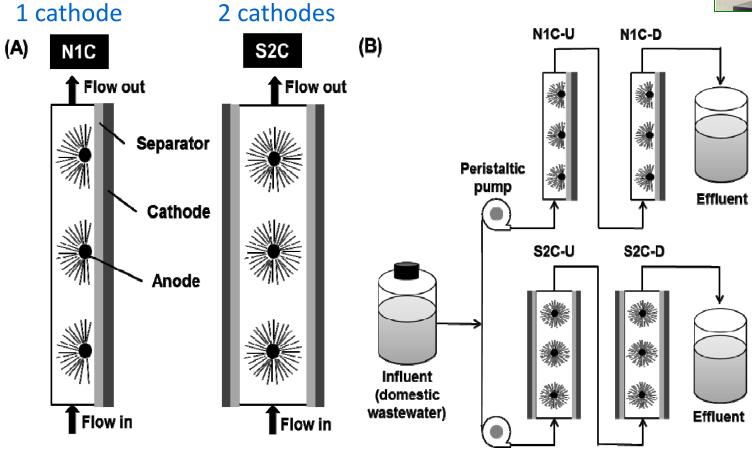


Maximum power densities similar for SEA & SPA



Gen 1 MFCs: 1 or 2 Cathodes?





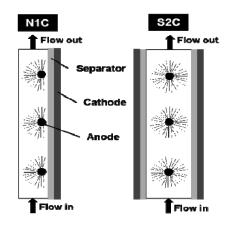
N1C=SEA (previous terminology)

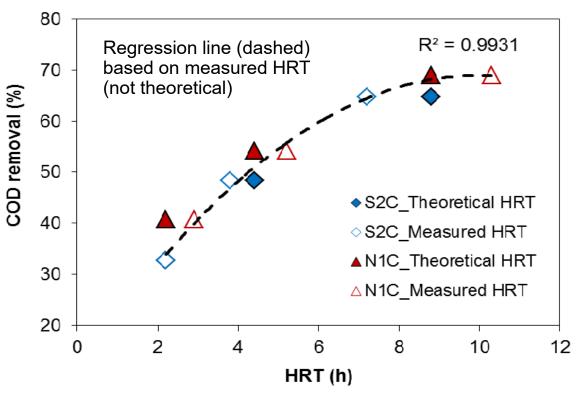


COD Removals vs actual HRTs

HRTs: N1C > S2C

- Same theoretical HRT set for reactor comparisons
- N1C > S2C

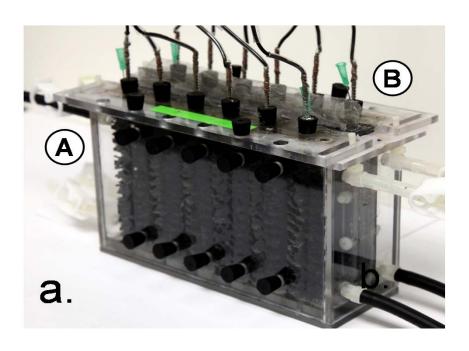


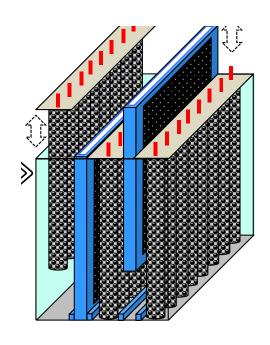


It is important to *measure* actual HRTs



Gen 2 MFCs: Design



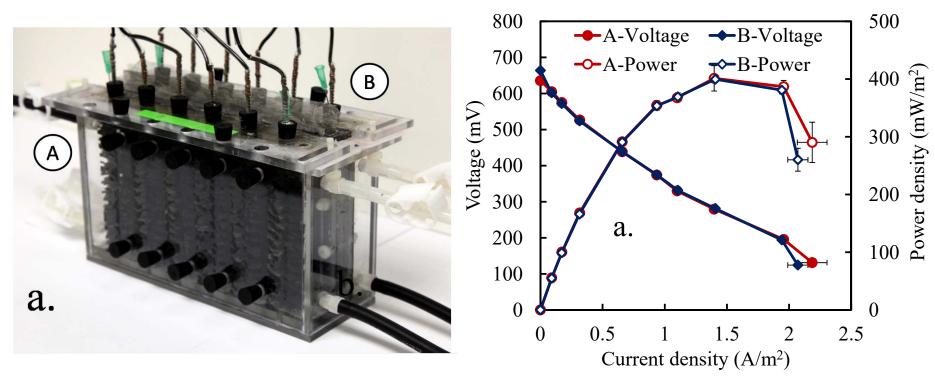


Modular MFC

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- Gen II reactor has 2 banks of 8 anodes; 2 cathodes
- Cathode specific surface area: 29 m² m⁻³ based on total liquid volume (1.4 L), or 20 m² m⁻³ based on total reactor volume (2 L).
- Not a "cassette" (anode+cathode) but <u>separate</u> anode and cathode modules.

Gen 2 MFCs: Power production



Modular MFC

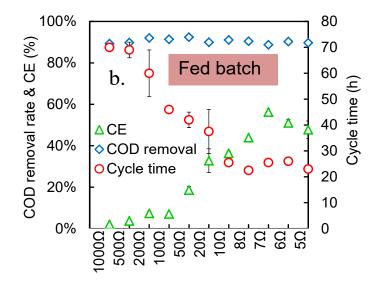
- Shown with 2 anodes, 2 cathodes; 20 m² m⁻³ (total volume)
- Produced ~ 400 mW/m² with domestic wastewater, highest to date for this source



Gen 2 MFCs: Performance

A a.

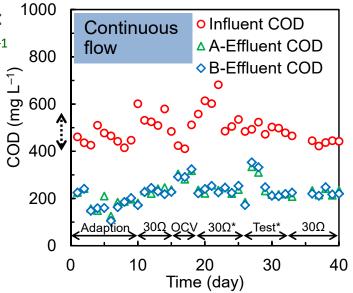
Fed batch: Long cycle times, high COD removal

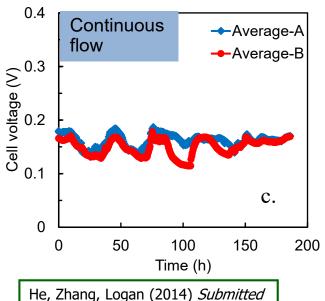




Influent: $480 \pm 25 \text{ mg L}^{-1}$

COD removal: $57 \pm 5\%$





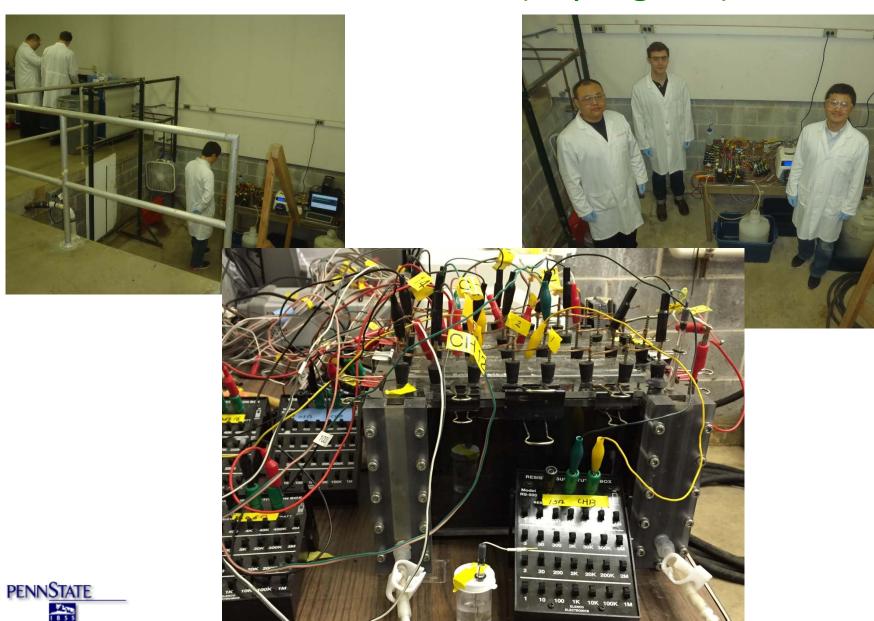


Power density comparisons: WW

Substrate	Notes	Power (mW/m²)	Reference
Domestic WW + Ac	Batch	1100	This study
Domestic WW	Batch	400	This study
Domestic WW	Cont. flow, 8 h HRT	250	This study
Domestic WW	25 mL, batch	332	Cheng&Logan
Domestic WW	25 mL, batch	130-240	Hays&Logan(2013)
Domestic WW	180 mL, Cont flow	280-330	Ahn et al (2014)
Domestic WW	180 mL, Batch	230	Yang et al. (2015)
Domestic WW	Cassette	100	Morio et al. (2013)
Domestic WW	Cassette	150	Yu et al. (2012)



Gen 3 MFCs (in progress)



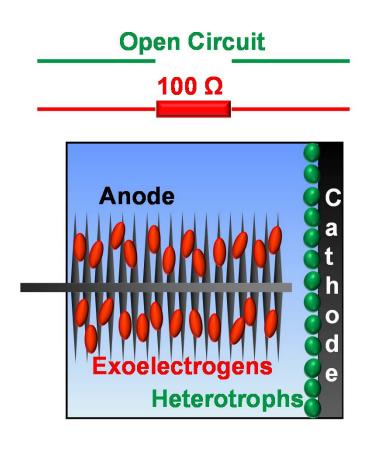


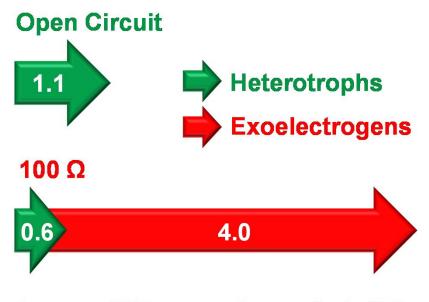
Final thoughts on using MFCs for Domestic Wastewater Treatment

- COD cannot be removed to < 30 mg/L with electricity generation
- A second process must be added after the MFC to further reduce COD
- Nutrient removal of anaerobic effluents is a research frontier (not just MFCs)



Current generation shifts more substrate to electricity generation in MFCs (acetate)





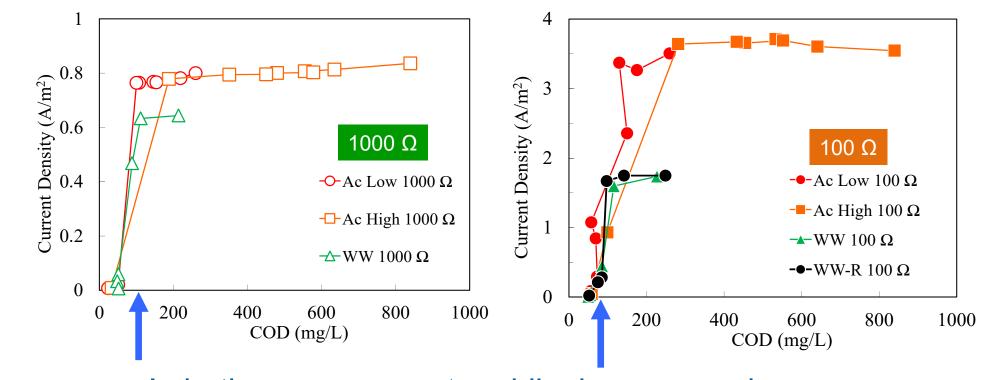
Average COD removal rates (kg/m³/d)

COD removal: 1st Order Reaction



Current density vs soluble COD (sCOD)

Current rapidly drops off at ~100 mg/L sCOD

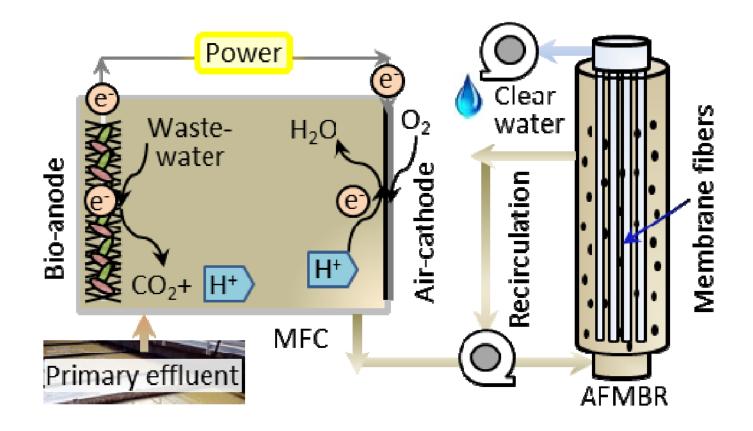


In both cases, current rapidly decreases when sCOD is still high (~100 mg/L)

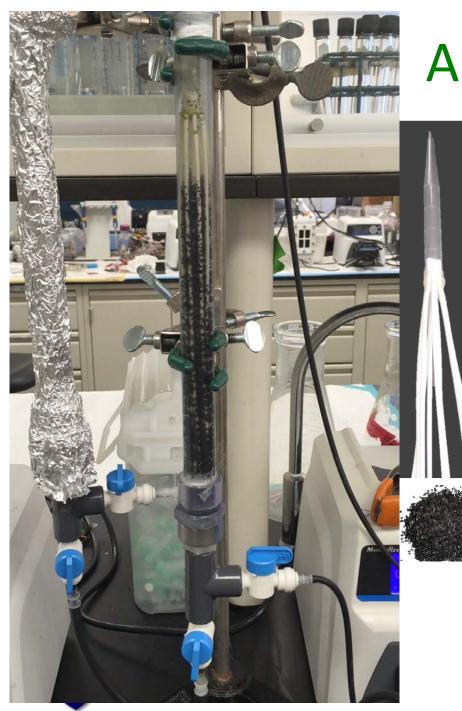


MFC + AFMBR

(Anaerobic Fluidized Bed Membrane Bioreactor)





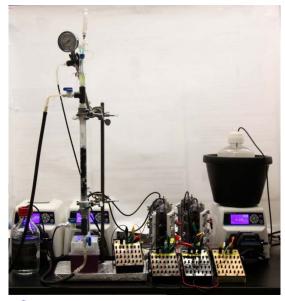


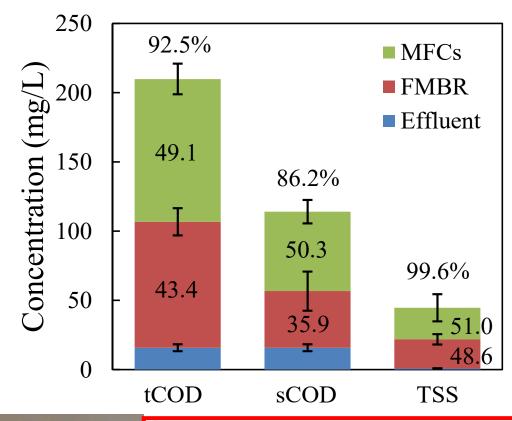
AFMBR Construction

- Idea of AFMBR first published by Chae et al. (ES&T). Used as a second stage to granular fluidized bed anerobic digester
- AFMBR consists of a reactor body + ultrafiltration membrane + granular activated carbon (GAC)
- GAC fluidized by recirculation
 - In tests here, used with a hydraulic retention time of 1 hour

Effluent reduced to 16 mg/L tCOD

- Two trains of MFC (HRT = 4 h)
 to AFMBR (HRT = 1 h)
- Membrane flux 16 L/m²/h
- 50 days performance
- Energy balanced (MFC produced = AFMBR used)







- Effluent COD = 16 mg/L
- Effluent TSS <1 mg/L



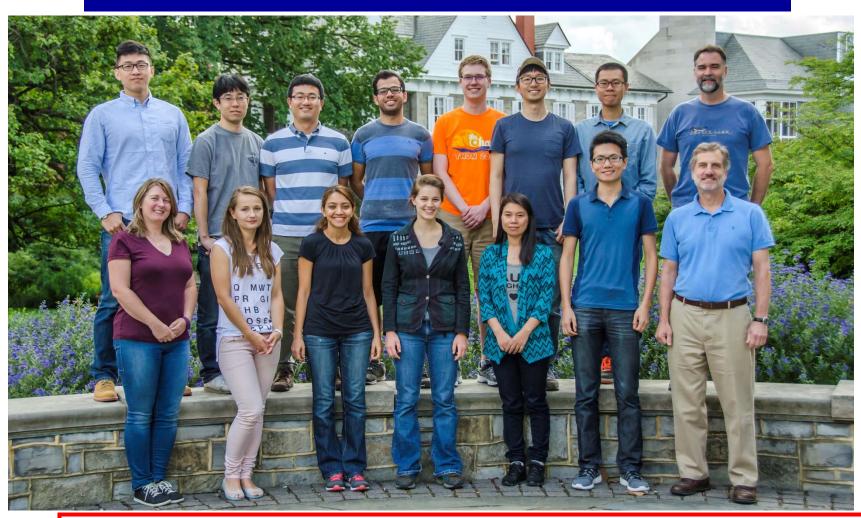
WW in AFMBR

Conclusions

- MFCs can be used for domestic wastewater treatment
 - Cost of electrodes reduce: to < \$40 m⁻²
 - High performance for brush anodes and activated carbon cathodes
 - Cathode specific surface area must be maintained as reactor sizes are increased
- A second process is needed for COD removal
 - Adding an AFMBR increased COD removal to achieve <20 mg/L
 - TSS < 1 mg/L, so no secondary clarifier needed
 - Nutrients need to be solved.



Thanks to students and researchers in the MxC team at Penn State!





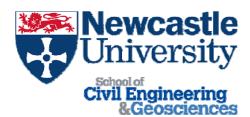
PENNSTATE | SERDP/DOD (2012-2015); GCEP/Stanford (2012-2015); NREL/DOE (2014-2017); NSF SusChem-EAGER (2015-2016)

International Collaborations















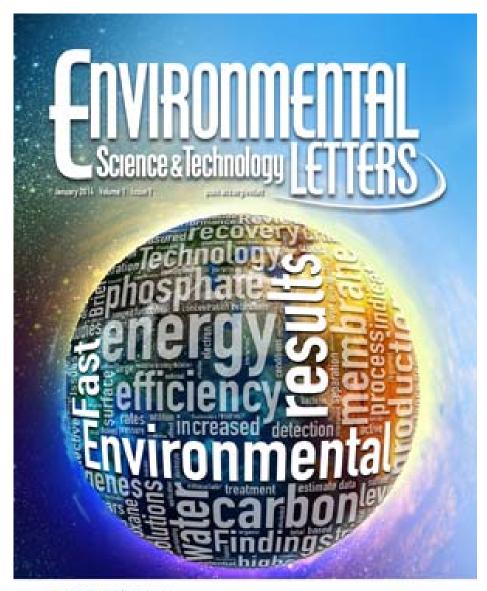














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