

QUADRATURE METHODS

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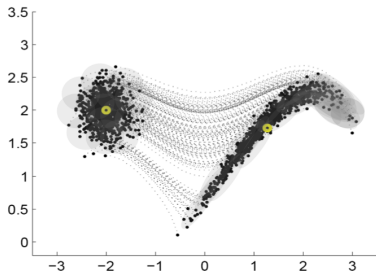


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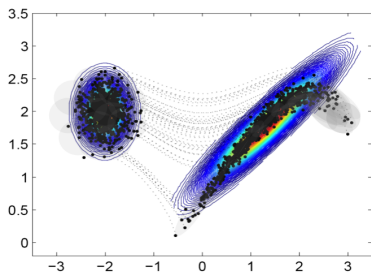


Workshop: New Advances in Uncertainty Analysis & Estimation
Air-force Research Laboratories, Kirtland, NM
July 18-19, 2017

Acknowledgement: N. Adurthi



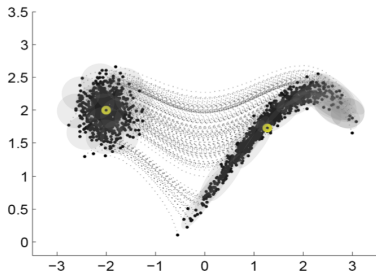
(a)



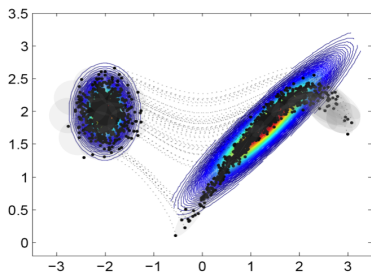
(b)

- **Different Approaches:** Kolmogorov Equation, Monte Carlo Methods, generalized Polynomial Chaos (gPC).
- All these methods involves the evaluation of expectation integrals:

$$E[f(\mathbf{x})] = \int \int \cdots \int p(\mathbf{x}) f(\mathbf{x}) d\mathbf{x} \approx \sum_{i=1}^n w_i f(\mathbf{x}_i)$$



(c)



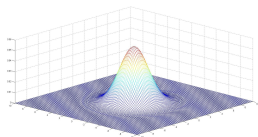
(d)

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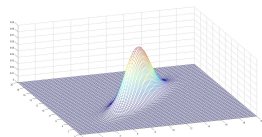
$$E[f(x)] = \int \int \cdots \int p(\mathbf{x}) f(\mathbf{x}) d\mathbf{x} \approx \sum_{i=1}^n w_i f(\mathbf{x}_i)$$

INTRODUCTION

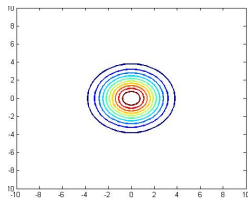
GAUSSIAN PDF UNDER LINEAR TRANSFORMATION



(e) pdf of x



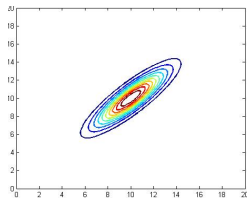
(a) pdf of y



(f) contours

LINEAR TRANSFORMATION

$$y = Ax + B$$



(b) contours

Figure: *Initial Gaussian pdf*

Figure: *Final Gaussian pdf*

ANALYTICAL MEAN AND COVARIANCE

$$E[y] = AE[x] + B$$

$$E[(y - E[y])(y - E[y])^T] = \Sigma_y = A\Sigma_x A^T$$

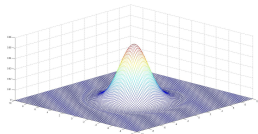


Figure: *Initial Gaussian pdf*

NONLINEAR TRANSFORMATION

$$y = f(x)$$

- Indirect information of the pdf
- No information about the shape of the pdf
- Can be easily evaluated by numerical integration

- 1 Computation of the pdf can be difficult.
- 2 Histogram can give some information about the shape.
- 3 Indirect information of the pdf: Statistics/Moments.

MOMENTS OF THE TRANSFORMED VARIABLE: FOR EXAMPLE IN THE 2D CASE

$$E[\mathbf{y}] = E[f(\mathbf{x})] = \int f(\mathbf{x})p(\mathbf{x}) d\mathbf{x}$$

$$E[y_1^{n_1} y_2^{n_2}] = \int f_1(\mathbf{x})^{n_1} f_2(\mathbf{x})^{n_2} p(\mathbf{x}) d\mathbf{x}$$

$$E[\mathbf{y}\mathbf{y}^T] = E[f(\mathbf{x})f(\mathbf{x})^T] = \int f(\mathbf{x})f(\mathbf{x})^T p(\mathbf{x}) d\mathbf{x}$$

MOTIVATION FOR USING MOMENTS

IN PERSPECTIVE OF DYNAMIC SYSTEMS

Dynamic System with uncertainty

$$\dot{x} = f(x, \rho) \quad \rho \sim p(\rho)$$

Solution for 1 set of parameters

$$x(t) = g(t, \rho^{(i)})$$

MOTIVATION FOR USING MOMENTS

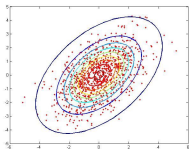
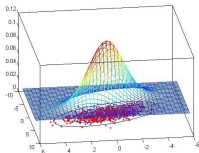
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Uncertainty pdf and contours of $p(\rho)$

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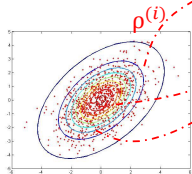
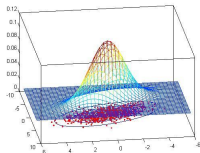
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N points

Uncertainty pdf and contours of $p(\rho)$

N evaluations

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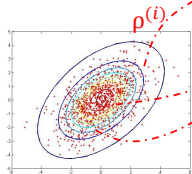
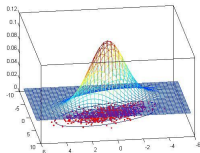
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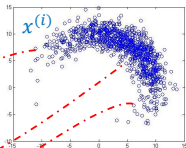
Solution for 1 set of parameters

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N points

Uncertainty pdf and contours of $p(\rho)$



MOTIVATION FOR USING MOMENTS

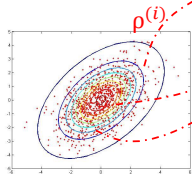
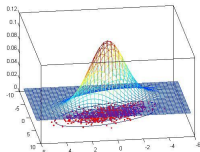
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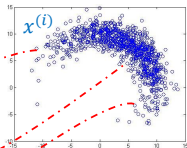
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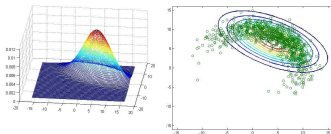


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Uncertainty pdf and contours of $p(\rho)$



N evaluations



Gaussian Approximation

$$\mu = \frac{1}{N} \sum_{i=1 \text{ to } N} x^{(i)} \quad \Sigma = \frac{1}{N} \sum_{i=1 \text{ to } N} (x^{(i)} - \mu)(x^{(i)} - \mu)^T$$

MOTIVATION FOR USING MOMENTS

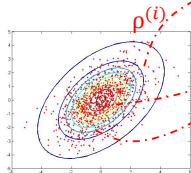
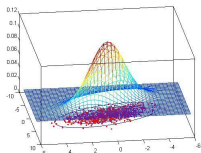
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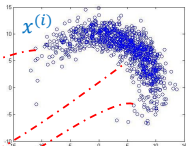
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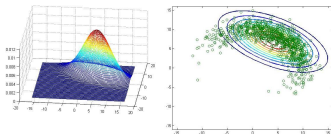


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Moment integral Approximation

$$\begin{aligned} \mu &= \int g(\rho) p(\rho) d\rho = \frac{1}{N} \sum_{i=1 \text{ to } N} x^{(i)} \\ \Sigma &= \int (g(\rho) - \mu)(g(\rho) - \mu)^T p(\rho) d\rho \end{aligned} \quad \left. \vphantom{\begin{aligned} \mu &= \int g(\rho) p(\rho) d\rho \\ \Sigma &= \int (g(\rho) - \mu)(g(\rho) - \mu)^T p(\rho) d\rho \end{aligned}} \right\} \begin{array}{l} \text{Gaussian Approximation} \\ \text{Moment integral Approximation} \end{array}$$

$$= \frac{1}{N} \sum_{i=1 \text{ to } N} (x^{(i)} - \mu)(x^{(i)} - \mu)^T$$

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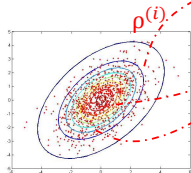
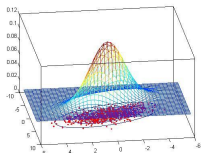
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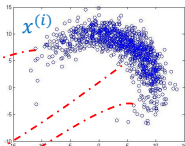
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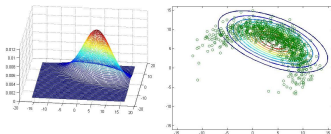


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$$= \frac{1}{N} \sum_{i=1}^N (x^{(i)} - \mu)(x^{(i)} - \mu)^T$$

$$E[x^n] = E[g(\rho)^n] = \int g(\rho)^n p(\rho) d\rho = \frac{1}{N} \sum g(\rho^{(i)})^n$$

More information with higher order moments

If direct shape is not important and only objective is to evaluate the moments, Monte Carlo runs can be avoided.

OBJECTIVE

$$E[f(\mathbf{x})] = \int \int \cdots \int p(\mathbf{x}) f(\mathbf{x}) d\mathbf{x} \approx \sum_{i=1}^N w_i f(\mathbf{x}_i)$$

Particularly, we are interested in

GAUSSIAN PDF $\Omega = [-\infty, \infty]$

$$p(\mathbf{x}) = \exp\left(-\frac{1}{2} \sum_{i=1}^n x_i^2\right)$$

- All the points are real.
- All the weights are real and positive

UNIFORM PDF $\Omega = [-1, 1]$

$$p(\mathbf{x}) = \frac{1}{2^n}$$

- The weights add to 1
- *All the points lie within the support of the pdf*

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MONTE CARLO METHODS

- Samples are drawn from the pdf $\mathbf{x}_i \sim p(\mathbf{x})$

The integral is approximated as an average of function evaluations at these samples

$$E[f(\mathbf{x})] = \frac{1}{N} \sum_{i=1}^N f(\mathbf{x}_i)$$

- The error $\propto \frac{1}{\sqrt{N}}$, where N is the number of samples.
- This is considered to be a slow in convergence.
- Hence often a large number of samples are required to get sufficient accuracy.

GAUSSIAN QUADRATURES

$$E[f(\mathbf{x})] = \sum_{i=1}^N w_i f(\mathbf{x}_i)$$

- The weights w_i and points \mathbf{x}_i are deterministic.
- *1-D integrals*: N quadrature points are required to reproduce the expectation integrals of a polynomial with degree $\leq 2N - 1$
- **n-D integrals**: Tensor product leads to exponential growth of points (N^n).

Gaussian pdf *Hermite Polynomials* – *Gauss-Hermite Quadrature*
Uniform pdf *Legendre Polynomials* – *Gauss-Legendre Quadrature*

EXPECTATION INTEGRAL

$$E[f(\mathbf{x})] = \int_{\Omega} f(\mathbf{x})p(\mathbf{x}) dx = \int \int \cdots \int f(\mathbf{x})p(\mathbf{x})dx_1dx_2 \cdots dx_n$$

EXPECTATION INTEGRAL

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TAYLOR SERIES

$$E[f(\mathbf{x})] \approx \sum_{N_1=0}^{\infty} \sum_{N_2=0}^{\infty} \cdots \sum_{N_n=0}^{\infty} \frac{E[x_1^{N_1}x_2^{N_2} \cdots x_n^{N_n}]}{N_1!N_2! \cdots N_n!} \frac{\partial^{N_1+N_2+\cdots+N_n} f}{\partial x_1^{N_1} \partial x_2^{N_2} \cdots \partial x_n^{N_n}}(\mathbf{0})$$

- The problem of evaluating the expected value of $f(\mathbf{x})$ has reduced to computing higher order moments of the pdf.
- Increasing the number of terms in the Taylor series expansion \Rightarrow Accurate evaluation of the expectation integral.

GAUSS-LEGENDRE QUADRATURE

POLYNOMIAL APPROXIMATION

TAYLOR SERIES

$$E[f(\mathbf{x})] \approx \sum_{N_1=0}^{\infty} \sum_{N_2=0}^{\infty} \cdots \sum_{N_n=0}^{\infty} \frac{E[x_1^{N_1} x_2^{N_2} \cdots x_n^{N_n}]}{N_1! N_2! \cdots N_n!} \frac{\partial^{N_1+N_2+\cdots+N_n} f}{\partial x_1^{N_1} \partial x_2^{N_2} \cdots \partial x_n^{N_n}}(\mathbf{0})$$

WEIGHTED APPROXIMATION

$$E[f(\mathbf{x})] \approx \sum_{i=1}^N w_i f(\mathbf{x}_i) \approx \sum_{N_1=0}^{\infty} \sum_{N_2=0}^{\infty} \cdots \sum_{N_n=0}^{\infty} \frac{(\sum_{i=1}^N w_i \{x_{(i,1)}^{N_1} x_{(i,2)}^{N_2} \cdots x_{(i,n)}^{N_n}\})}{N_1! N_2! \cdots N_n!} \frac{\partial^{N_1+N_2+\cdots+N_n} f}{\partial x_1^{N_1} \partial x_2^{N_2} \cdots \partial x_n^{N_n}}(\mathbf{0})$$

COMPARING COEFFICIENTS OF $f(\mathbf{0})$ & ITS DERIVATIVES

$$\sum_{i=1}^N w_i \{x_{(i,1)}^{N_1} x_{(i,2)}^{N_2} \cdots x_{(i,n)}^{N_n}\} = E[x_1^{N_1} x_2^{N_2} \cdots x_n^{N_n}]$$

We just need to match moments in input space, \mathbf{x}

EXPECTATION INTEGRAL

$$E[f(x)] = \int_{\Omega} f(x)p(x) dx$$

EXPECTATION INTEGRAL

$$E[f(x)] = \int_{\Omega} f(x)p(x) dx$$

If $p(x) = \mathcal{N}(x; 0, 1)$ and $\Omega = (-\infty, \infty)$, the moments of the **Gaussian pdf** are

$$E[1] = 1, \quad E[x] = 0, \quad E[x^2] = 1, \quad E[x^3] = 0, \quad E[x^4] = 3$$

So, if $f(x) = P_3(x) = a_3x^3 + a_2x^2 + a_1x + a_0$

$$\begin{aligned} \int_{\Omega} f(x)p(x) dx &= \int_{\Omega} P_3(x)\mathcal{N}(x; 0, 1) dx \\ &= \int_{\Omega} a_3x^3 \mathcal{N}(x; 0, 1) dx + \int_{\Omega} a_2x^2 \mathcal{N}(x; 0, 1) dx + \int_{\Omega} a_1x \mathcal{N}(x; 0, 1) dx + \int_{\Omega} a_0 \mathcal{N}(x; 0, 1) dx \\ &= a_3E[x^3] + a_2E[x^2] + a_1E[x] + a_0E[1] \quad (\text{Integrating Polynomials} \Rightarrow \text{Capturing moments}) \\ &= a_0 + a_2 \end{aligned}$$

EXPECTATION INTEGRAL

$$E[f(x)] = \int_{\Omega} f(x)p(x) dx$$

If $p(x) = \frac{1}{2}$ and $\Omega = [-1, 1]$, the moments of the **Uniform pdf** are:

$$E[1] = 1, \quad E[x] = 0, \quad E[x^2] = \frac{1}{3}, \quad E[x^3] = 0, \quad E[x^4] = \frac{1}{5}$$

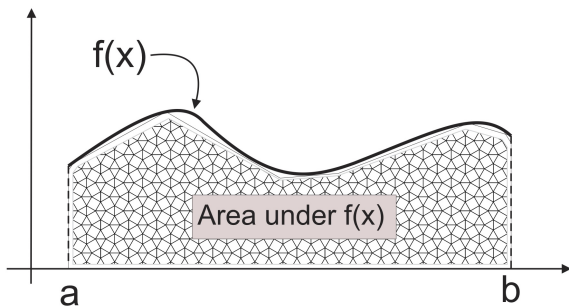
So, if $f(x) = P_3(x) = a_3x^3 + a_2x^2 + a_1x + a_0$

$$\begin{aligned} \int_{\Omega} f(x)p(x) dx &= \int_{\Omega} P_3(x) \frac{1}{2} dx \\ &= \int_{\Omega} a_3x^3 \frac{1}{2} dx + \int_{\Omega} a_2x^2 \frac{1}{2} dx + \int_{\Omega} a_1x \frac{1}{2} dx + \int_{\Omega} a_0 \frac{1}{2} dx \\ &= \frac{a_3}{2} E[x^3] + \frac{a_2}{2} E[x^2] + \frac{a_1}{2} E[x] + \frac{a_0}{2} E[1] \quad (\text{Integrating Polynomials} \Rightarrow \text{Capturing moments}) \\ &= \frac{a_0}{2} + \frac{a_2}{6} \end{aligned}$$

EXPECTATION INTEGRAL

$$E[f(x)] = \int_{\Omega} f(x)p(x) dx$$

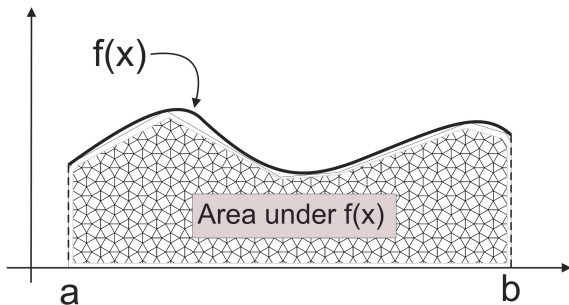
i.e. it is required to find the area under the curve $f(x)$



GAUSS-LEGENDRE QUADRATURE

POLYNOMIAL APPROXIMATION

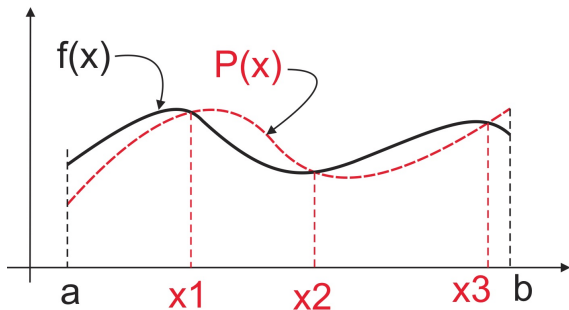
Given the function $f(x)$



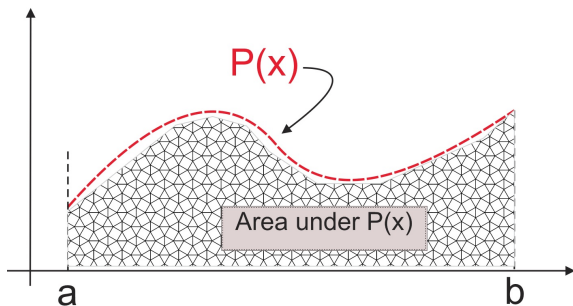
GAUSS-LEGENDRE QUADRATURE

POLYNOMIAL APPROXIMATION

Approximate $f(x)$ by a polynomial $P(x)$



Integrate the polynomial $P(x)$



For example consider the 3rd order polynomial approximation:

$$P_3(x) = a_3x^3 + a_2x^2 + a_1x + a_0$$

4 variables \Rightarrow 4 equations are needed. Consider 2 points x_1 and x_2

$$f(x_1) = P_3(x_1) = a_3x_1^3 + a_2x_1^2 + a_1x_1 + a_0$$

$$f(x_2) = P_3(x_2) = a_3x_2^3 + a_2x_2^2 + a_1x_2 + a_0$$

$$f'(x_1) = P_3'(x_1) = 3a_3x_1^2 + 2a_2x_1 + a_1$$

$$f'(x_2) = P_3'(x_2) = 3a_3x_2^2 + 2a_2x_2 + a_1$$

Solve for a_0, a_1, a_2, a_3

$$a_0 = \frac{f(x_2)x_1^2(x_1 - 3x_2) + x_2(f(x_1)(3x_1 - x_2)x_2 - x_1(x_1 - x_2)(x_2f'(x_1) + x_1f'(x_2)))}{(x_1 - x_2)^3}$$

$$a_1 = \frac{-6f(x_1)x_1x_2 + 6f(x_2)x_1x_2 + (x_1 - x_2)(x_2^2f'(x_1) + x_1^2f'(x_2) + 2x_1x_2(f'(x_1) + f'(x_2)))}{(x_1 - x_2)^3}$$

$$a_2 = \frac{3f(x_1)(x_1 + x_2) - 3f(x_2)(x_1 + x_2) - (x_1 - x_2)(x_2(2f'(x_1) + f'(x_2)) + x_1(f'(x_1) + 2f'(x_2)))}{(x_1 - x_2)^3}$$

$$a_3 = \frac{-2f(x_1) + 2f(x_2) + (x_1 - x_2)(f'(x_1) + f'(x_2))}{(x_1 - x_2)^3}$$

EXPECTATION INTEGRAL

POLYNOMIAL APPROXIMATION

For **Gaussian pdf**

$$\int_{\Omega} f(x) dx \approx \int_{\Omega} P_3(x) dx = a_2 + a_0$$

Force the coefficients of $f'(x_1)$ and $f'(x_2)$ to 0

$$\frac{2x_2 + x_1(1 + x_2^2)}{(x_1 - x_2)^2} = 0 \quad \frac{2x_1 + x_2 + x_1^2 x_2}{(x_1 - x_2)^2} = 0$$

$$x_1 = -1$$

$$x_2 = 1$$

$$w_1 = \frac{1}{2}$$

$$w_2 = \frac{1}{2}$$

x_1 and x_2 are exactly the roots of the 2nd order **Hermite Polynomial**
 $x^2 - 1$

For **Uniform pdf**

$$\int_{-1}^1 f(x) dx \approx \int_{-1}^1 P_3(x) dx = 2a_0 + \frac{2a_2}{3}$$

Force the coefficients of $f'(x_1)$ and $f'(x_2)$ to 0

$$\frac{2x_2 + x_1(1 + 3x_2^2)}{3(x_1 - x_2)^2} = 0 \quad \frac{2x_1 + x_2 + 3x_1^2 x_2}{3(x_1 - x_2)^2} = 0$$

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x_1 and x_2 are exactly the roots of the 2nd order **Legendre polynomial**
 $\frac{1}{2}(3x^2 - 1) = 0$

EXPECTATION INTEGRAL

POLYNOMIAL APPROXIMATION

For **Gaussian pdf**

$$\begin{aligned}\int_{\Omega} f(x) dx &\approx \int_{\Omega} P_3(x) dx = a_2 + a_0 \\ &= \frac{(3x_2^2 - x_2^3 + 3x_1(1+x_2^2))}{(x_1-x_2)^3} f(x_1) + \frac{(-3x_1+x_1^3-3x_2-3x_1^2x_2)}{(x_1-x_2)^3} f(x_2) \\ &\quad - \frac{2x_2+x_1(1+x_2^2)}{(x_1-x_2)^2} f'(x_1) - \frac{2x_1+x_2+x_1^2x_2}{(x_1-x_2)^2} f'(x_2)\end{aligned}$$

Force the coefficients of $f'(x_1)$ and $f'(x_2)$ to 0

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 $x^2 - 1$

For **Uniform pdf**

$$\begin{aligned}\int_{-1}^1 f(x) dx &\approx \int_{-1}^1 P_3(x) dx = 2a_0 + \frac{2a_2}{3} \\ &= \frac{2(x_2-x_2^3+x_1(1+3x_2^2))}{(x_1-x_2)^3} f(x_1) + \frac{2(-x_1+x_1^3-x_2-3x_1^2x_2)}{(x_1-x_2)^3} f(x_2) \\ &\quad - 2\frac{2x_2+x_1(1+3x_2^2)}{3(x_1-x_2)^2} f'(x_1) - 2\frac{2x_1+x_2+3x_1^2x_2}{3(x_1-x_2)^2} f'(x_2)\end{aligned}$$

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EXPECTATION INTEGRAL

POLYNOMIAL APPROXIMATION

For **Gaussian pdf**

$$\int_{\Omega} f(x) dx \approx \int_{\Omega} P_3(x) dx = a_2 + a_0$$

$$= \underbrace{\frac{(3x_2^2 - x_2^3 + 3x_1(1 + x_2^2))}{(x_1 - x_2)^3}}_{w_1} f(x_1) + \underbrace{\frac{(-3x_1 + x_1^3 - 3x_2 - 3x_1^2 x_2)}{(x_1 - x_2)^3}}_{w_2} f(x_2)$$

$$- \underbrace{\frac{2x_2 + x_1(1 + x_2^2)}{(x_1 - x_2)^2}}_0 f'(x_1) - \underbrace{\frac{2x_1 + x_2 + x_1^2 x_2}{(x_1 - x_2)^2}}_0 f'(x_2)$$

Force the coefficients of $f'(x_1)$ and $f'(x_2)$ to 0

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For **Uniform pdf**

$$\int_{-1}^1 f(x) dx \approx \int_{-1}^1 P_3(x) dx = 2a_0 + \frac{2a_2}{3}$$

$$= \underbrace{\frac{2(x_2 - x_2^3 + x_1(1 + 3x_2^2))}{(x_1 - x_2)^3}}_{w_1} f(x_1) + \underbrace{\frac{2(-x_1 + x_1^3 - x_2 - 3x_1^2 x_2)}{(x_1 - x_2)^3}}_{w_2} f(x_2)$$

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EXPECTATION INTEGRAL

POLYNOMIAL APPROXIMATION

For **Gaussian pdf**

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EXPECTATION INTEGRAL

POLYNOMIAL APPROXIMATION

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EXPECTATION INTEGRAL

POLYNOMIAL APPROXIMATION

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x_1 and x_2 are exactly the roots of the 2nd order **Legendre polynomial**

$$\frac{1}{2}(3x^2 - 1) = 0$$

Hence, for Gaussian quadratures, one only needs

- 2 points to integrate all polynomials of degree 3 or less

The procedure can be repeated using a 5th order polynomial with 6 coefficients. One can use 3 function evaluations and 3 function derivative evaluations at 3 points to form 6 equations. This way one has

- 3 points to integrate all polynomials of degree 5 or less

In general Gaussian Quadratures only need

- N points to integrate all polynomials of degree $2N - 1$ or less

$p(x) \sim \text{Gaussian}$ *Hermite Polynomial* *Gauss – Hermite Quadrature*
 $p(x) \sim \text{Uniform}$ *Legendre Polynomial* *Gauss – Legendre Quadrature*

GAUSS-LEGENDRE QUADRATURE

POLYNOMIAL APPROXIMATION

- Alternatively, one can use Nested Quadrature such as Clenshaw-Curtis¹ Quadrature
- Higher order points make use of lower order points (*hence nested*)
- Clenshaw curtis needs $N - 1$ points to integrate polynomials of degree N or less
- Gaussian Quadratures need N points to integrate polynomials of degree $2N - 1$ or less

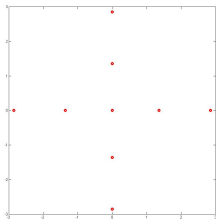


Figure: 1D points

*Higher dimension Gaussian Quadrature are constructed from **Tensor product** of 1D points*

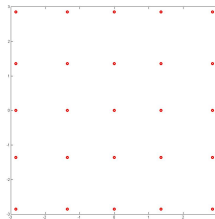


Figure: 2D points

¹Trefethen, Lloyd N. "Is Gauss quadrature better than Clenshaw-Curtis?." SIAM review 50.1 (2008): 67-87.

SPARSE GRID QUADRATURE

SMOLYAK SCHEME

$$Q_k^{(n)} = \sum ((Q_i^{(1)} - Q_{i-1}^{(1)}) \otimes Q_{k-i+1}^{(n-1)}) [f]$$

- $Q_k^{(n)}$ is the sparse grid rule of dimension n and of $2k - 1$ degree exactness.
- where $Q_i^{(1)}$ is the 1D Gaussian Quadrature rule with i points.
- The Smolyak sparse grid scheme¹ has fewer points than the Gaussian Quadrature Product rule.

¹T. Gerstner and M. Griebel. "Numerical integration using sparse grids." Numerical algorithms 18.3-4 (1998): 209-232.

²A. H. Stroud, "Approximate Calculation of Multiple Integrals," Prentice Hall, 1971.

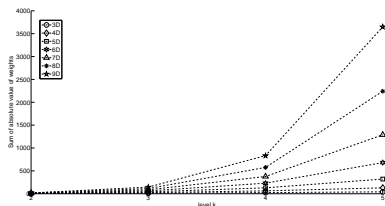


Figure: Sum of absolute value of the weights

- This algorithm can contain **negative weights**.
- If $\sum |w_i| \gg 1$, then the quadrature rule introduces large **roundoff errors**².

SPARSE GRID QUADRATURE

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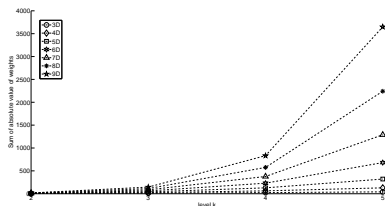
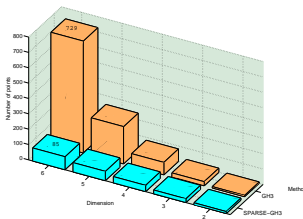


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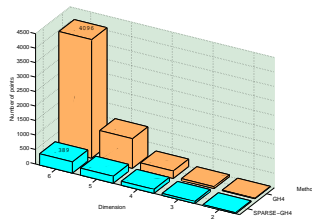
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SPARSE GRID QUADRATURE

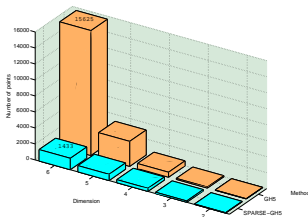
SMOLYAK SCHEME



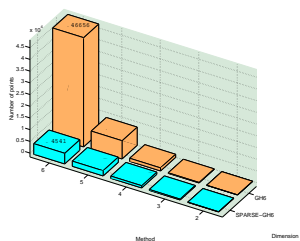
(a) Polynomial exactness 5 or less



(b) Polynomial exactness 7 or less



(c) Polynomial exactness 9 or less



(d) Polynomial exactness 11 or less

THE UNSCENTED TRANSFORMATION

3rd-DEGREE CUBATURE RULE

- Developed specifically for the Gaussian pdf.
- 3rd order rule with $2n + 1$ points.
- Can integrate all odd degree monomials due to symmetry of the points chosen.
- The tuning parameter κ is selected such that $n + \kappa = 3$. This makes the central weight negative after dimension 3.
- The points are constrained to be on the orthogonal axes (or Principal axes).

UNSCENTED TRANSFORM

$$X_0 = (0, \dots, 0)$$

$$W_0 = \kappa / (n + \kappa)$$

$$X_i = \sqrt{(n + \kappa)} I_i$$

$$W_i = 1 / [2(n + \kappa)]$$

$$X_{i+n} = -\sqrt{(n + \kappa)} I_i$$

$$W_{i+n} = 1 / [2(n + \kappa)]$$

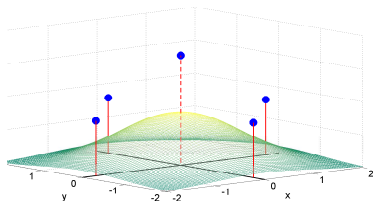


Figure: Selection of points in 2D

S. Julier, J. Uhlmann, H. F. Durrant-Whyte, "A new method for the nonlinear transformation of means and covariances in filters and estimators," Automatic Control, IEEE Transactions on , vol.45, no.3, March 2000.

Assuming i.i.d Gaussian random variables $\mathbf{x} = [x_1, x_2, \dots, x_n]^T$ with zero mean and identity covariance, the higher order moments up to fourth order are given as:

MOMENTS OF A GAUSSIAN PDF

$$E[x_i^2] = 1,$$

$$E[x_i x_j] = 0,$$

$$E[x_i^4] = 3$$

$$E[x_i^3 x_j] = 0,$$

$$E[x_i^2 x_j^2] = 1,$$

$$E[x_i^2 x_j x_k] = 0$$

$$E[x_i x_j x_k x_l] = 0,$$

The central point on the origin (mean) has weight w_0 . When enumerated the set of points are $\{(r_1, 0, \dots, 0), (0, r_1, \dots, 0), (0, 0, \dots, r_1), (-r_1, 0, \dots, 0), (0, -r_1, \dots, 0), (0, 0, \dots, -r_1), (0, 0, \dots, 0)\}$ and all the points have the same weight w_1 . The corresponding MCE upto 4th order are:

$$E[x_i^0] \equiv w_0 + 2nw_1 = 1$$

$$E[x_i^4] \equiv 2r_1^4 w_1 = 3$$

$$E[x_i^2] \equiv 2r_1^2 w_1 = 1$$

$$E[x_i^2 x_j^2] \equiv 0 \neq 1$$

The cross order moment cannot be satisfied with this choice of points (as all points have only one non-zero coordinate)

$$E[x_i^0] \equiv w_0 + 2nw_1 = 1$$

$$E[x_i^2] \equiv 2r_1^2 w_1 = 1$$

$$E[x_i^4] \equiv 2r_1^4 w_1 = 3$$

From the 3rd equation, w_1 can be solved as:

$$w_1 = \frac{1}{2r_1^2} \Rightarrow r_1 = \sqrt{3}$$

$$\Rightarrow w_1 = \frac{1}{6}$$

$$\Rightarrow w_0 = 1 - \frac{n}{3}$$

Negative central weight after dimension 3

Alternatively, choose $r_1 = \sqrt{n + \kappa}$, where κ is a parameter and n is dimension

$$w_1 = \frac{1}{2(n + \kappa)}$$

$$w_0 = 1 - 2nw_1 = 1 - \frac{n}{n + \kappa} = \frac{\kappa}{n + \kappa}$$

$$2r_1^2 w_1 = 2(n + \kappa)^2 \frac{1}{2(n + \kappa)} = n + \kappa = 3$$

$n + \kappa = 3$ to capture only one 4th order moment, however, central weight becomes negative for $n > 3$.

$$E[x_i^0] \equiv w_0 + 2nw_1 = 1$$

$$E[x_i^2] \equiv 2r_1^2 w_1 = 1$$

$$E[x_i^4] \equiv 2r_1^4 w_1 = 3$$

From the 3rd equation, w_1 can be solved as:

$$w_1 = \frac{1}{2r_1^2} \Rightarrow r_1 = \sqrt{3}$$

$$\Rightarrow w_1 = \frac{1}{6}$$

$$\Rightarrow w_0 = 1 - \frac{n}{3}$$

Negative central weight after dimension 3

Alternatively, choose $r_1 = \sqrt{n + \kappa}$, where κ is a parameter and n is dimension

$$w_1 = \frac{1}{2(n + \kappa)}$$

$$w_0 = 1 - 2nw_1 = 1 - \frac{n}{n + \kappa} = \frac{\kappa}{n + \kappa}$$

$$2r_1^2 w_1 = 2(n + \kappa)^2 \frac{1}{2(n + \kappa)} = n + \kappa = 3$$

$n + \kappa = 3$ to capture only one 4th order moment, however, central weight becomes negative for $n > 3$.

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$$w_0 = 1 - 2nw_1 = 1 - \frac{n}{n + \kappa} = \frac{\kappa}{n + \kappa}$$

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$$w_1 = \frac{1}{2(n + \kappa)}$$

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$$2r_1^2 w_1 = 2(n + \kappa)^2 \frac{1}{2(n + \kappa)} = n + \kappa = 3$$

$n + \kappa = 3$ to capture only one 4th order moment, however, central weight becomes negative for $n > 3$.

THE UNSCENTED TRANSFORMATION

3rd-DEGREE CUBATURE RULE

- For zero mean and identity covariance Gaussian pdf: the points on the perpendicular cartesian axes can be represented as
- $(\pm r_1, 0, \dots, 0)$, $(0, \pm r_1, \dots, 0) \dots$, $(0, 0, \dots, \pm r_1)$ and $(0, 0, \dots, 0)$.
- Any cross order moment such as $E[x_1^2 x_2^2]$ becomes zero by such selection of points.
- One would have to *'look for additional axes that are able to capture higher order moments'*

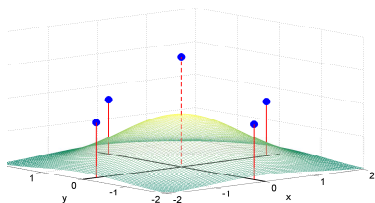


Figure: Unscented Transform for 2D

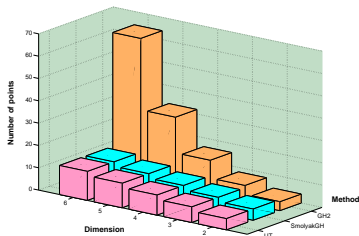


Figure: Comparison of 3rd degree rules

MOMENT CONSTRAINT EQUATIONS(MCEs):

$$\sum_{i=1}^N w_i \{x_{(i,1)}^{n_1} x_{(i,2)}^{n_2} \cdots x_{(i,n)}^{n_n}\} = E[x_1^{n_1} x_2^{n_2} \cdots x_N^{n_n}]$$

A FULLY SYMMETRIC SET

A set of points is called fully symmetric if it is closed under all coordinate and sign permutations.

- For example consider the set $\mathbf{X} = \{\mathbf{x}_1, \mathbf{x}_2, \dots\}$ to be a fully symmetric set and if $\mathbf{x}_i = [a, b]^T \in \mathbf{X}$, then $\{[b, a]^T, [-a, b]^T, [a, -b]^T, [-a, -b]^T, [-b, a]^T, [b, -a]^T, [-b, -a]^T\} \in \mathbf{X}$.

CONJUGATE UNSCENTED TRANSFORMATION

DEFINITIONS

σ : Represents the *Principal axes* (or orthogonal axis) in the cartesian coordinate space. Each point on the principal axis is denoted as σ_i

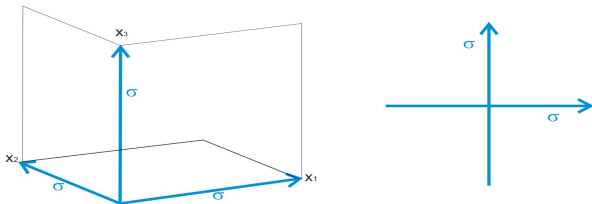


TABLE: Fully Symmetric set of points

Type	Sample Point	No. of points
σ	$(1, 0, 0, \dots, 0)$	$2n$
σ^M	$(\underbrace{1, 1, \dots, 1}_M, \underbrace{0, 0, \dots, 0}_{n-M})$	$2^M \binom{n}{M}$
σ^n	$(0, 1, 1, \dots, 1)$	$n2^n$

CONJUGATE UNSCENTED TRANSFORMATION

DEFINITIONS

c^M : Represents the M^{th} Conjugate axes (fully symmetric set) and the corresponding points are enumerated as c_i^M

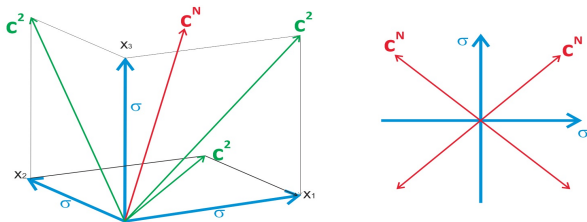


TABLE: Fully Symmetric set of points

Type	Sample Point	No. of points
σ	$(1, 0, 0, \dots, 0)$	$2n$
c^M	$(\underbrace{1, 1, \dots, 1}_M, \underbrace{0, 0, \dots, 0}_{n-M})$	$2^M \binom{n}{M}$
	$(0, 1, 1, \dots, 1)$	2^M

CONJUGATE UNSCENTED TRANSFORMATION

DEFINITIONS

$s^N(h)$: Represents the *Scaled Conjugate axes* and the points are denoted as $s_i^N(h)$. The parameter h is a scaling factor.

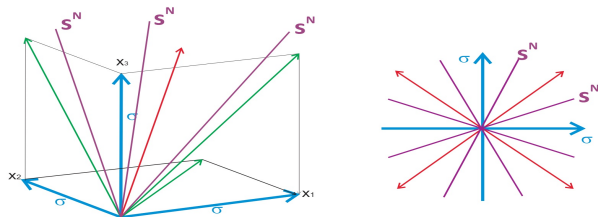
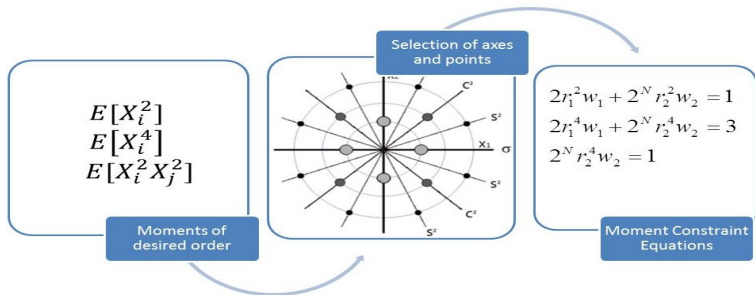
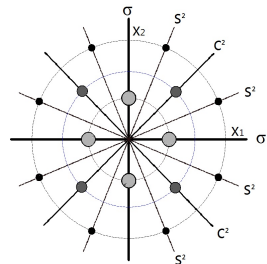
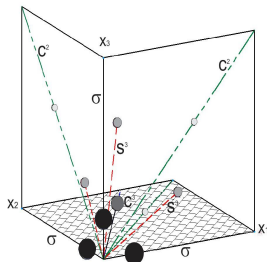


TABLE: Fully Symmetric set of points

Type	Sample Point	No. of points
σ	$(1, 0, 0, \dots, 0)$	$2n$
c^M	$(\underbrace{1, 1, \dots, 1}_M, \underbrace{0, 0, \dots, 0}_{n-M})$	$2^M \binom{n}{M}$
$s^N(h)$	$(h, 1, 1, \dots, 1)$	$n2^{n-1}$

CONJUGATE UNSCENTED TRANSFORMATION

GRAPHICAL VISUALIZATION OF THE POINTS/AXES



EVEN MOMENTS

GAUSSIAN PDF AND UNIFORM PDF

Let $[x_1, \dots, x_i, \dots, x_j, \dots, x_k, \dots, x_l, \dots, x_n]$ be a n-dimensional random vector

GAUSSIAN PDF

Moment	value	Moment	value	Moment	value
$E[x_i^2]$	1	$E[x_i^4]$	3	$E[x_i^2 x_j^2]$	1
$E[x_i^6]$	15	$E[x_i^4 x_j^2]$	3	$E[x_i^2 x_j^2 x_k^2]$	1
$E[x_i^8]$	105	$E[x_i^6 x_j^2]$	15	$E[x_i^4 x_j^4]$	9
$E[x_i^4 x_j^2 x_k^2]$	3	$E[x_i^2 x_j^2 x_k^2 x_l^2]$	1		

UNIFORM PDF

Moment	value	Moment	value		
$E[x_i^2]$	$\frac{1}{3}$	$E[x_i^4]$	$\frac{1}{5}$	$E[x_i^2 x_j^2]$	$\frac{1}{9}$
$E[x_i^6]$	$\frac{1}{7}$	$E[x_i^4 x_j^2]$	$\frac{1}{15}$	$E[x_i^2 x_j^2 x_k^2]$	$\frac{1}{27}$
$E[x_i^8]$	$\frac{1}{9}$	$E[x_i^6 x_j^2]$	$\frac{1}{21}$	$E[x_i^4 x_j^4]$	$\frac{1}{25}$
$E[x_i^4 x_j^2 x_k^2]$	$\frac{1}{45}$	$E[x_i^2 x_j^2 x_k^2 x_l^2]$	$\frac{1}{81}$		

TABLE: Fully Symmetric set of points for CUT4

Dimension	σ	c^2	c^3	c^4	c^5	c^6	c^7	c^8	c^9	s^n
2	4	4	-	-	-	-	-	-	-	8
3	6	12	8	-	-	-	-	-	-	24
4	8	24	32	16	-	-	-	-	-	64
5	10	40	80	80	32	-	-	-	-	160
6	12	60	160	240	192	64	-	-	-	384
7	14	84	280	560	672	448	128	-	-	896
8	16	112	448	1120	1792	1792	1024	256	-	2048
9	18	144	672	2016	4032	5376	4608	2304	512	4608

Choosing points as

- $\sigma : (\pm r_1, 0, 0, \dots, 0)$ with weight w_1
- $c^2 : (\pm r_2, \pm r_2, 0, \dots, 0)$ with weight w_2

$$E[x_i^2] \equiv 2r_1^2 w_1 + 4(n-1)r_2^2 w_2 = 1$$

$$E[x_i^4] \equiv 2r_1^4 w_1 + 4(n-1)r_2^4 w_2 = 3$$

$$E[x_i^2 x_j^2] \equiv 4r_2^4 w_2 = 1$$

$$E[x_i^0] \equiv 1 - 2nw_1 - 2n(n-1)w_2 = w_0$$

$$w_2 = \frac{1}{4r_2^4}, \quad w_1 = \frac{4-n}{2r_1^4}$$

$$r_1^2 r_2^2 = r_1^2 (n-1) + r_2^2 (4-n)$$

TABLE: Fully Symmetric set of points for CUT4

Dimension	σ	c^2	c^3	c^4	c^5	c^6	c^7	c^8	c^9	s^n
2	4	4	-	-	-	-	-	-	-	8
3	6	12	8	-	-	-	-	-	-	24
4	8	24	32	16	-	-	-	-	-	64
5	10	40	80	80	32	-	-	-	-	160
6	12	60	160	240	192	64	-	-	-	384
7	14	84	280	560	672	448	128	-	-	896
8	16	112	448	1120	1792	1792	1024	256	-	2048
9	18	144	672	2016	4032	5376	4608	2304	512	4608

Choosing points as

- $\sigma : (\pm r_1, 0, 0, \dots, 0)$ with weight w_1
- $c^2 : (\pm r_2, \pm r_2, 0, \dots, 0)$ with weight w_2

$$E[x_i^2] \equiv 2r_1^2 w_1 + 4(n-1)r_2^2 w_2 = 1$$

$$E[x_i^4] \equiv 2r_1^4 w_1 + 4(n-1)r_2^4 w_2 = 3$$

$$E[x_i^2 x_j^2] \equiv 4r_2^4 w_2 = 1$$

$$E[x_i^0] \equiv 1 - 2nw_1 - 2n(n-1)w_2 = w_0$$

$$w_2 = \frac{1}{4r_2^4}, \quad w_1 = \frac{4-n}{2r_1^4}$$

$$r_1^2 r_2^2 = r_1^2 (n-1) + r_2^2 (4-n)$$

TABLE: Fully Symmetric set of points for CUT4²

Dimension	σ	c^2	c^3	c^4	c^5	c^6	c^7	c^8	c^9	s^n
2	4	4	-	-	-	-	-	-	-	8
3	6	12	8	-	-	-	-	-	-	24
4	8	24	32	16	-	-	-	-	-	64
5	10	40	80	80	32	-	-	-	-	160
6	12	60	160	240	192	64	-	-	-	384
7	14	84	280	560	672	448	128	-	-	896
8	16	112	448	1120	1792	1792	1024	256	-	2048
9	18	144	672	2016	4032	5376	4608	2304	512	4608

Choosing points as

- $\sigma : (\pm r_1, 0, 0, \dots, 0)$ with weight w_1
- $c^n : (\pm r_2, \pm r_2, \dots, \pm r_2)$ with weight w_2

$$r_1 = \sqrt{\frac{n+2}{2}},$$

$$w_1 = \frac{1}{r_1^4} = \frac{4}{(n+2)^2},$$

$$E[x_i^2] \equiv 2r_1^2 w_1 + 2^n r_2^2 w_2 = 1$$

$$E[x_i^4] \equiv 2r_1^4 w_1 + 2^n r_2^4 w_2 = 3$$

$$E[x_i^2 x_j^2] \equiv 2^n r_2^4 w_2 = 1$$

$$E[x_i^0] \equiv 1 - 2n w_1 - 2^n w_2 = w_0$$

$$r_2 = \sqrt{\frac{n+2}{n-2}}$$

$$w_2 = \frac{1}{2^n r_2^4} = \frac{(n-2)^2}{2^n (n+2)^2}$$

²N. Adhurthi, P. Singla and T. Singh, "The Conjugate Unscented Transform - An Approach to Evaluate Multi-Dimensional Expectation Integrals," *2012 American Control Conference, Montréal, Canada, June 27-June 29, 2012.*

TABLE: Fully Symmetric set of points for CUT6

Dimension	σ	c^2	c^3	c^4	c^5	c^6	c^7	c^8	c^9	s^n
2	4	4	-	-	-	-	-	-	-	8
3	6	12	8	-	-	-	-	-	-	24
4	8	24	32	16	-	-	-	-	-	64
5	10	40	80	80	32	-	-	-	-	160
6	12	60	160	240	192	64	-	-	-	384
7	14	84	280	560	672	448	128	-	-	896
8	16	112	448	1120	1792	1792	1024	256	-	2048
9	18	144	672	2016	4032	5376	4608	2304	512	4608

Choosing points as

- $\sigma : (\pm r_1, 0, 0, \dots, 0)$ with weight w_1
- $c^n : (\pm r_2, \pm r_2, \dots, \pm r_2)$ with weight w_2
- $c^2 : (\pm r_3, \pm r_3, 0, \dots, 0)$ with weight w_3
- Numerical solvers for polynomial system of equations can be exploited to solve these equations.

$$2r_1^2 w_1 + 2^n r_2^2 w_2 + 4(n-1)r_3^2 w_3 = 1$$

$$2r_1^4 w_1 + 2^n r_2^4 w_2 + 4(n-1)r_3^4 w_3 = 3$$

$$2^n r_2^4 w_2 + 4r_3^4 w_3 = 1$$

$$2r_1^6 w_1 + 2^n r_2^6 w_2 + 4(n-1)r_3^6 w_3 = 15$$

$$2^n r_2^6 w_2 + 4r_3^6 w_3 = 3$$

$$2^n r_2^6 w_2 = 1$$

$$1 - 2n w_1 - 2^n w_2 - 2n(n-1)w_3 = w_0$$

TABLE: Fully Symmetric set of points for CUT8

Dimension	σ	c^2	c^3	c^4	c^5	c^6	c^7	c^8	c^9	s^n
2	4	4	-	-	-	-	-	-	-	8
3	6	12	8	-	-	-	-	-	-	24
4	8	24	32	16	-	-	-	-	-	64
5	10	40	80	80	32	-	-	-	-	160
6	12	60	160	240	192	64	-	-	-	384

Choosing points as

- $\sigma : (\pm r_1, 0, 0, \dots, 0)$ with weight w_1 .
- $c^n : (\pm r_2, \pm r_2, \dots, \pm r_2)$ with weight w_2 .
- $c^2 : (\pm r_3, \pm r_3, 0, \dots, 0)$ with weight w_3 .
- $c^n : (\pm r_4, \pm r_4, \dots, \pm r_4)$ with weight w_4 .
- $c^3 : (\pm r_5, \pm r_5, \pm r_5, 0, \dots, 0)$ with weight w_5 .
- $s^n : (\pm h r_6, \pm r_6, \dots, \pm r_6)$ with weight w_6 .
- 11 equations and 13 variables.
- Tractable solution obtained by assuming values for h .
- Solved by Numerical polynomial system solvers such as BERTINI.
- Choose the real and positive solutions.

$$2r_1^2 w_1 + 32r_2^2 w_2 + 16r_3^2 w_3 + 32r_4^2 w_4 + 48r_5^2 w_5 + 128r_6^2 w_6 + 32h^2 r_6^2 w_6 = 1$$

$$2r_1^4 w_1 + 32r_2^4 w_2 + 16r_3^4 w_3 + 32r_4^4 w_4 + 48r_5^4 w_5 + 128r_6^4 w_6 + 32h^4 r_6^4 w_6 = 3$$

$$32r_2^4 w_2 + 4r_3^4 w_3 + 32r_4^4 w_4 + 24r_5^4 w_5 + 96r_6^4 w_6 + 64h^4 r_6^4 w_6 = 1$$

$$2r_1^6 w_1 + 32r_2^6 w_2 + 16r_3^6 w_3 + 32r_4^6 w_4 + 48r_5^6 w_5 + 128r_6^6 w_6 + 32h^6 r_6^6 w_6 = 15$$

$$32r_2^6 w_2 + 4r_3^6 w_3 + 32r_4^6 w_4 + 24r_5^6 w_5 + 96r_6^6 w_6 + 32h^2 r_6^6 w_6 + 32h^4 r_6^6 w_6 = 3$$

$$32r_2^6 w_2 + 32r_4^6 w_4 + 8r_5^6 w_5 + 64r_6^6 w_6 + 96h^2 r_6^6 w_6 = 1$$

$$2r_1^8 w_1 + 32r_2^8 w_2 + 16r_3^8 w_3 + 32r_4^8 w_4 + 48r_5^8 w_5 + 128r_6^8 w_6 + 32h^8 r_6^8 w_6 = 105$$

$$32r_2^8 w_2 + 4r_3^8 w_3 + 32r_4^8 w_4 + 24r_5^8 w_5 + 96r_6^8 w_6 + 32h^2 r_6^8 w_6 + 32h^4 r_6^8 w_6 = 15$$

$$32r_2^8 w_2 + 4r_3^8 w_3 + 32r_4^8 w_4 + 24r_5^8 w_5 + 96r_6^8 w_6 + 64h^4 r_6^8 w_6 = 9$$

$$32r_2^8 w_2 + 32r_4^8 w_4 + 8r_5^8 w_5 + 64r_6^8 w_6 + 64h^2 r_6^8 w_6 + 32h^4 r_6^8 w_6 = 3$$

$$32r_2^8 w_2 + 32r_4^8 w_4 + 32r_6^8 w_6 + 128h^2 r_6^8 w_6 = 1$$

CONJUGATE UNSCENTED TRANSFORMATION

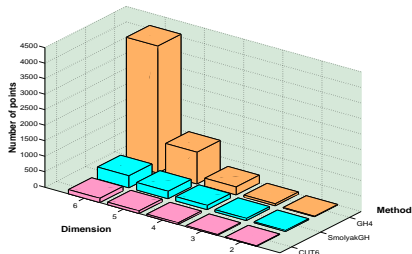
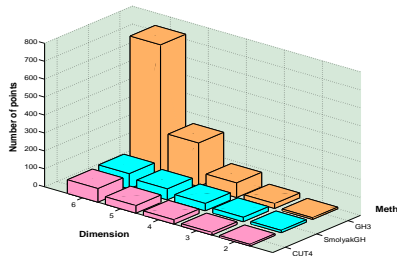
CUBATURE POINTS FOR 4th/5th AND 6th/7th DEGREE

TABLE: CUT4

	Position	Weights
$1 \leq i \leq 2N$	$X_i = r_1 \sigma_i$	$W_i = w_1$
$1 \leq i \leq 2^N$	$X_{i+2N} = r_2 c_i^N$	$W_{i+2N} = w_2$
Central weight	$X_0 = \mathbf{0}$	$W_0 = w_0$
$n = 2N + 2^N (+1)$		

TABLE: CUT6, ($N \leq 6$)

	Position	Weights
$1 \leq i \leq 2N$	$X_i = r_1 \sigma_i$	$W_i = w_1$
$1 \leq i \leq 2^N$	$X_{i+2N} = r_2 c_i^N$	$W_{i+2N} = w_2$
$1 \leq i \leq 2N(N-1)$	$X_{i+2N+2N} = r_3 c_i^2$	$W_{i+2N+2N} = w_3$
Central weight	$X_0 = \mathbf{0}$	$W_0 = w_0$
$n = 2N^2 + 2^N + 1$		



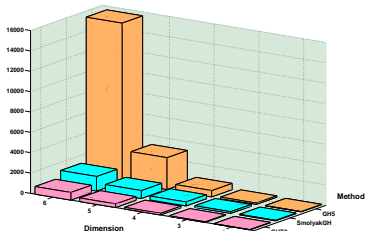
N. Adhurthi et al., "The Conjugate Unscented Transform - An Approach to Evaluate Multi-Dimensional Expectation Integrals," 2012 ACC.

CONJUGATE UNSCENTED TRANSFORMATION

CUBATURE POINTS FOR $8^{th}/9^{th}$ DEGREE

TABLE: Sigma Points for CUT8, ($2 \leq N \leq 6$)

	Position	Weights
$1 \leq i \leq 2N$	$X_i = r_1 \sigma_i$	$W_i = w_1$
$1 \leq i \leq 2^N$	$X_{i+2N} = r_2 c_i^N$	$W_{i+2N} = w_2$
$1 \leq i \leq 2N(N-1)$	$X_{i+2N+2N} = r_3 c_i^2$	$W_{i+2N+2N} = w_3$
$1 \leq i \leq 2^N$	$X_{i+2N+2^N+2N(N-1)} = r_4 c_i^N$	$W_{i+2N+2^N+2N(N-1)} = w_4$
$1 \leq i \leq N_1$	$X_{i+2N+2^N+2N(N-1)+2^N} = r_5 c_i^3$	$W_{i+2N+2^N+2N(N-1)+2^N} = w_5$
$1 \leq i \leq N2^N$	$X_{i+2N+2^N+2N(N-1)+2^N+N_1} = r_6 s_i^N$	$W_{i+2N+2^N+2N(N-1)+2^N+N_1} = w_6$
Central weight	$X_0 = \mathbf{0}$	$W_0 = w_0$
$n = 2N + 2^N + 2N(N-1) + N_1 + 2^N + N2^N + 1, \{N_1 = 4N(N-1)(N-2)/3\}$		



CONJUGATE UNSCENTED TRANSFORMATION

CUT4- MOMENTS UPTO 4th ORDER- UNIFORM PDF

The moments Constraint equations up to 4th order are:

$$E[x_i^0] = 1 \Rightarrow \sum_{i=1}^n w_i = 1 \qquad E[x_i^2] = \frac{1}{3} \Rightarrow \sum_{i=1}^n w_i x_i^2 = \frac{1}{3}$$

$$E[x_i^4] = \frac{1}{5} \Rightarrow \sum_{i=1}^n w_i x_i^4 = \frac{1}{5} \qquad E[x_i^2 x_j^2] = \frac{1}{9} \Rightarrow \sum_{i=1}^n w_i x_i^2 x_j^2 = \frac{1}{9}$$

- Choosing 1 set of points on σ_1 with weight w_1 and 1 set of points on σ_2 with weight w_2 .

- The moment constraint equations become:

- $2Nw_1 + 2^N w_2 = 1 \quad 2r_1^2 w_1 + 2^N r_2^2 w_2 = \frac{1}{3},$

- $2r_1^4 w_1 + 2^N r_2^4 w_2 = \frac{1}{5} \quad 2^N r_2^4 w_2 = \frac{1}{9}$

The equations can be analytically solved as

$$r_1 = \sqrt{\frac{4+5N}{30}} \quad w_1 = \frac{40}{(4+5N)^2} \quad r_2 = \sqrt{\frac{4+5N}{-12+15N}} \quad w_2 = \frac{(4-5N)^2}{2^N(4+5N)^2}$$

CONJUGATE UNSCENTED TRANSFORMATION

CUT4- MOMENTS UPTO 4th ORDER- UNIFORM PDF

The moments Constraint equations up to 4th order are:

$$E[x_i^0] = 1 \Rightarrow \sum_{i=1}^n w_i = 1 \qquad E[x_i^2] = \frac{1}{3} \Rightarrow \sum_{i=1}^n w_i x_i^2 = \frac{1}{3}$$

$$E[x_i^4] = \frac{1}{5} \Rightarrow \sum_{i=1}^n w_i x_i^4 = \frac{1}{5} \qquad E[x_i^2 x_j^2] = \frac{1}{9} \Rightarrow \sum_{i=1}^n w_i x_i^2 x_j^2 = \frac{1}{9}$$

- Choosing 1 set of points on σ_i with weight w_i and 1 set of points on c_i^N with weight w_2 .
- The moment constraint equations become:

- $2Nw_1 + 2^N w_2 = 1 \quad 2r_1^2 w_1 + 2^N r_2^2 w_2 = \frac{1}{3}$,

- $2r_1^4 w_1 + 2^N r_2^4 w_2 = \frac{1}{5} \quad 2^N r_2^4 w_2 = \frac{1}{9}$

The equations can be analytically solved as

$$r_1 = \sqrt{\frac{4+5N}{30}} \quad w_1 = \frac{40}{(4+5N)^2} \quad r_2 = \sqrt{\frac{4+5N}{-12+15N}} \quad w_2 = \frac{(4-5N)^2}{2^N(4+5N)^2}$$

CONJUGATE UNSCENTED TRANSFORMATION

CUT4- MOMENTS UPTO 4th ORDER- UNIFORM PDF

The moments Constraint equations up to 4th order are:

$$E[x_i^0] = 1 \Rightarrow \sum_{i=1}^n w_i = 1 \qquad E[x_i^2] = \frac{1}{3} \Rightarrow \sum_{i=1}^n w_i x_i^2 = \frac{1}{3}$$

$$E[x_i^4] = \frac{1}{5} \Rightarrow \sum_{i=1}^n w_i x_i^4 = \frac{1}{5} \qquad E[x_i^2 x_j^2] = \frac{1}{9} \Rightarrow \sum_{i=1}^n w_i x_i^2 x_j^2 = \frac{1}{9}$$

- Choosing 1 set of points on σ_i with weight w_i and 1 set of points on c_i^N with weight w_2 .
- The moment constraint equations become:

- $2Nw_1 + 2^N w_2 = 1 \quad 2r_1^2 w_1 + 2^N r_2^2 w_2 = \frac{1}{3},$

- $2r_1^4 w_1 + 2^N r_2^4 w_2 = \frac{1}{5} \quad 2^N r_2^4 w_2 = \frac{1}{9}$

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$$r_1 = \sqrt{\frac{4+5N}{30}} \quad w_1 = \frac{40}{(4+5N)^2} \quad r_2 = \sqrt{\frac{4+5N}{-12+15N}} \quad w_2 = \frac{(4-5N)^2}{2^N(4+5N)^2}$$

CONJUGATE UNSCENTED TRANSFORMATION

CUT4- MOMENTS UPTO 4th ORDER- UNIFORM PDF

The moments Constraint equations up to 4th order are:

$$E[x_i^0] = 1 \Rightarrow \sum_{i=1}^n w_i = 1 \qquad E[x_i^2] = \frac{1}{3} \Rightarrow \sum_{i=1}^n w_i x_i^2 = \frac{1}{3}$$

$$E[x_i^4] = \frac{1}{5} \Rightarrow \sum_{i=1}^n w_i x_i^4 = \frac{1}{5} \qquad E[x_i^2 x_j^2] = \frac{1}{9} \Rightarrow \sum_{i=1}^n w_i x_i^2 x_j^2 = \frac{1}{9}$$

- Choosing 1 set of points on σ_i with weight w_i and 1 set of points on c_i^N with weight w_2 .
- The moment constraint equations become:
- $2Nw_1 + 2^N w_2 = 1 \quad 2r_1^2 w_1 + 2^N r_2^2 w_2 = \frac{1}{3},$
- $2r_1^4 w_1 + 2^N r_2^4 w_2 = \frac{1}{5} \quad 2^N r_2^4 w_2 = \frac{1}{9}$

The equations can be analytically solved as

$$r_1 = \sqrt{\frac{4+5N}{30}} \quad w_1 = \frac{40}{(4+5N)^2} \quad r_2 = \sqrt{\frac{4+5N}{-12+15N}} \quad w_2 = \frac{(4-5N)^2}{2^N(4+5N)^2}$$

CONJUGATE UNSCENTED TRANSFORMATION

CUT4- MOMENTS UPTO 4th ORDER- UNIFORM PDF

The moments Constraint equations up to 4th order are:

$$E[x_i^0] = 1 \Rightarrow \sum_{i=1}^n w_i = 1 \qquad E[x_i^2] = \frac{1}{3} \Rightarrow \sum_{i=1}^n w_i x_i^2 = \frac{1}{3}$$

$$E[x_i^4] = \frac{1}{5} \Rightarrow \sum_{i=1}^n w_i x_i^4 = \frac{1}{5} \qquad E[x_i^2 x_j^2] = \frac{1}{9} \Rightarrow \sum_{i=1}^n w_i x_i^2 x_j^2 = \frac{1}{9}$$

- Choosing 1 set of points on σ_i with weight w_i and 1 set of points on c_i^N with weight w_2 .
- The moment constraint equations become:
- $2Nw_1 + 2^N w_2 = 1 \quad 2r_1^2 w_1 + 2^N r_2^2 w_2 = \frac{1}{3},$
- $2r_1^4 w_1 + 2^N r_2^4 w_2 = \frac{1}{5} \quad 2^N r_2^4 w_2 = \frac{1}{9}$

The equations can be analytically solved as

$$r_1 = \sqrt{\frac{4+5N}{30}} \quad w_1 = \frac{40}{(4+5N)^2} \quad r_2 = \sqrt{\frac{4+5N}{-12+15N}} \quad w_2 = \frac{(4-5N)^2}{2^N(4+5N)^2}$$

CONJUGATE UNSCENTED TRANSFORMATION

CUT4- MOMENTS UPTO 4th ORDER- UNIFORM PDF

The moments Constraint equations up to 4th order are:

$$E[x_i^0] = 1 \Rightarrow \sum_{i=1}^n w_i = 1 \qquad E[x_i^2] = \frac{1}{3} \Rightarrow \sum_{i=1}^n w_i x_i^2 = \frac{1}{3}$$

$$E[x_i^4] = \frac{1}{5} \Rightarrow \sum_{i=1}^n w_i x_i^4 = \frac{1}{5} \qquad E[x_i^2 x_j^2] = \frac{1}{9} \Rightarrow \sum_{i=1}^n w_i x_i^2 x_j^2 = \frac{1}{9}$$

- Choosing 1 set of points on σ_i with weight w_i and 1 set of points on c_i^N with weight w_2 .
- The moment constraint equations become:
- $2Nw_1 + 2^N w_2 = 1 \quad 2r_1^2 w_1 + 2^N r_2^2 w_2 = \frac{1}{3},$
- $2r_1^4 w_1 + 2^N r_2^4 w_2 = \frac{1}{5} \quad 2^N r_2^4 w_2 = \frac{1}{9}$

The equations can be analytically solved as

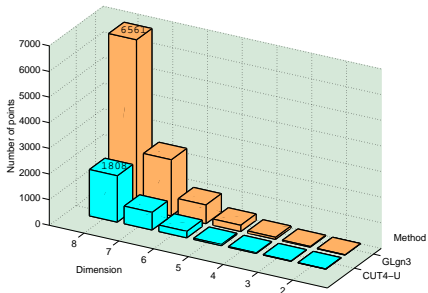
$$r_1 = \sqrt{\frac{4+5N}{30}} \quad w_1 = \frac{40}{(4+5N)^2} \quad r_2 = \sqrt{\frac{4+5N}{-12+15N}} \quad w_2 = \frac{(4-5N)^2}{2^N(4+5N)^2}$$

CONJUGATE UNSCENTED TRANSFORMATION

CUBATURE POINTS FOR 4th/5th - UNIFORM PDF

TABLE: CUT4-U rules

N	Point Selection	
2,3,4,5	$r_1 \sigma_i$	$r_2 c_i^N$
	w_1	w_2
6	$r_1 \sigma_i$	$r_2 c_i^4$
	w_1	w_2
7,8	$r_1 \sigma_i$	$r_2 c_i^5$
	w_1	w_2



N. Adurthi, P. Singla and T. Singh, "Conjugate Unscented Transform Rules for Uniform Probability Density Functions," 2013 American Control Conference, Washington D.C., June 17–19, 2013.

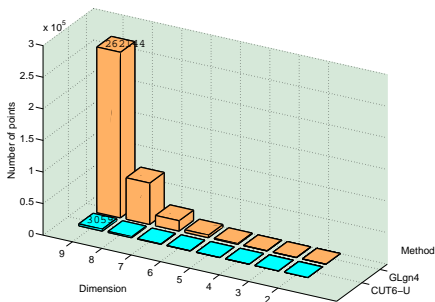
N. Adurthi, P. Singla and T. Singh, "Conjugate Unscented Transformation: Applications to Estimation and Control," ASME Journal of Dynamics, Measurements and Control, 2017.

CONJUGATE UNSCENTED TRANSFORMATION

CUBATURE POINTS FOR 6th/7th DEGREE- UNIFORM PDF

TABLE: CUT6-U rules

N	Point Selection			
2	$r_1 \sigma_i$	$r_2 c_i^N$	$r_3 c_i^N$	-
	w_1	w_2	w_3	-
3,4	$r_1 \sigma_i$	$r_2 c_i^N$	$r_3 c_i^2$	$r_4 c_i^N$
	w_1	w_2	w_3	w_4
5,6,7	$r_1 \sigma_i$	$r_2 c_i^N$	$r_3 c_i^3$	$r_4 c_i^N$
	w_1	w_2	w_3	w_4
8,9	$r_1 \sigma_i$	$r_2 c_i^N$	$r_3 c_i^4$	$r_4 c_i^N$
	w_1	w_2	w_3	w_4

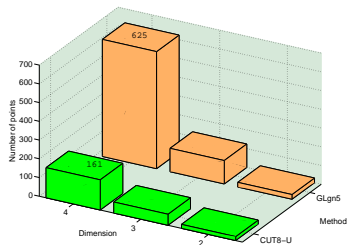


CONJUGATE UNSCENTED TRANSFORMATION

CUBATURE POINTS FOR 8th/9th - UNIFORM PDF

TABLE: CUT4-U rules

N	Point Selection					
2	$r_1 \sigma_i$	$r_2 c_i^2$	$r_3 s_i^N(h)$	$r_4 c_i^2$	-	-
	w_1	w_2	w_3	w_4	-	-
3	$r_1 \sigma_i$	$r_2 c_i^N$	$r_3 c_i^2$	$r_4 c_i^N$	$r_5 s_i^N(h)$	-
	w_1	w_2	w_3	w_4	w_5	-
4	$r_1 \sigma_i$	$r_2 c_i^N$	$r_3 c_i^2$	$r_4 c_i^3$	$r_5 s_i^N(h)$	$r_6 c_i^N$
	w_1	w_2	w_3	w_4	w_5	w_6
5	$r_1 \sigma_i$	$r_2 c_i^N$	$r_3 c_i^2$	$r_4 c_i^3$	$r_5 s_i^N(h)$	$r_6 c_i^N$
	w_1	w_2	w_3	w_4	w_5	w_6



CONJUGATE UNSCENTED TRANSFORMATION

COMPARING QUADRATURE METHODS

TABLE: Number of Points for 5th order accurate cubature methods.

Dim	GH		GHS		KPS		CUT4-G		HCKF-5	
	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N
2	1	<u>9</u>	5	13	1	<u>9</u>	1	<u>9</u>	1	<u>9</u>
3	1	27	13	25	1	19	1	14	1	19
4	1	81	25	41	1	33	1	24	1	33
5	1	243	41	61	2.11	51	1	42	1.2041	51
6	1	729	61	85	3.67	73	1	<u>76</u>	1.37	73
7	1	2187	85	113	5.67	99	1	<u>142</u>	1.52	99
8	1	6561	113	145	8.11	129	1	<u>272</u>	1.64	129
9	1	19683	145	181	11	163	1	<u>530</u>	1.74	163

$\mathbf{N} \Rightarrow$ minimal number of quadrature points, $\underline{\mathbf{N}} \Rightarrow$ minimal number of quadrature points with positive weight.

Gauss-Hermite Quadrature (GH), Gauss Hermite Smolyak quadrature (GHS), Kronrod Patterson Smolyak quadrature (KPS), High order cubature Kalman filter (HCKF)

CONJUGATE UNSCENTED TRANSFORMATION

COMPARING QUADRATURE METHODS

TABLE: Number of Points for 7th order accurate cubature points.

<i>Dim</i>	GH		GHS		KPS		CUT6-G		HCKF-7	
	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N
2	1	16	7	29	1	17	1	<u>13</u>	1	24
3	1	64	25	69	1.654	39	1	<u>27</u>	1	76
4	1	256	63	137	2.293	81	1	<u>49</u>	1	176
5	1	1024	129	241	2.931	151	1	<u>83</u>	1	340
6	1	4096	231	389	4.754	257	1	<u>137</u>	1.56	584
7	1	16384	377	589	7.614	407	1	<u>423</u>	2.1	924
8	1	65536	575	849	11.808	609	1	<u>721</u>	2.57	1376
9	1	262144	833	1177	17.63	871	1	<u>1203</u>	3.01	1956

$\mathbf{N} \Rightarrow$ minimal number of quadrature points, $\underline{\mathbf{N}} \Rightarrow$ minimal number of quadrature points with positive weight.

Gauss-Hermite Quadrature (GH), Gauss Hermite Smolyak quadrature (GHS), Kronrod Patterson Smolyak quadrature (KPS), High order cubature Kalman filter (HCKF)

CONJUGATE UNSCENTED TRANSFORMATION

COMPARING QUADRATURE METHODS

TABLE: Number of Points for 9th order accurate cubature points.

<i>Dim</i>	GH		GHS		KPS		CUT8-G	
	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N	$\sum w_i $	N
2	1	25	9	53	1.485	37	1	<u>21</u>
3	1	125	41	165	2.6360	93	1	<u>59</u>
4	1	625	129	385	3.825	201	1	<u>161</u>
5	1	3125	321	781	4.95	401	1	<u>355</u>
6	1	15625	681	1433	6.07	749	1	<u>745</u>

N \Rightarrow minimal number of quadrature points, **N** \Rightarrow minimal number of quadrature points with positive weight.

Gauss-Hermite Quadrature (GH), Gauss Hermite Smolyak quadrature (GHS), Kronrod Patterson Smolyak quadrature (KPS), High order cubature Kalman filter (HCKF)

$$Q = \int 0.1 \sum_{i=1}^6 x_i^8 \mathcal{N}(x; 0, I) dx$$

TABLE: True Value of Integral=63.

Method	Q_{approx}	min(w)	$\sum w_i $	N
<i>UT</i>	205.8000	0.0714	1	13
<i>HCKF-5</i>	-28.8000	-0.0156	1.3750	73
<i>CUT4-G</i>	21.6000	0.0039	1	76
<i>CUT6-G</i>	60.5981	8.2885e-004	1	137
<i>CUT8-G</i>	63.0000	7.8492e-005	1	745
<i>GH3</i>	16.2000	2.1433e-005	1	729
<i>GH4</i>	48.6000	9.3219e-009	1	4096
<i>GH5</i>	63.0000	2.0353e-012	1	15625
<i>GH6</i>	63.0000	2.7871e-016	1	46656
<i>GH7</i>	63.0000	2.7162e-020	1	117649
<i>GH8</i>	63.0000	2.0397e-024	1	262144
<i>GHS3</i>	16.2000	-2.5000	61	85
<i>GHS4</i>	48.6000	-30.0000	231	389
<i>GHS5</i>	63.0000	-13.3333	681	1433
<i>GHS6</i>	63.0000	-90.3333	1683	4541
<i>GHS7</i>	63.0000	-34.9444	3653	12841
<i>GHS8</i>	63.0000	-199.3439	7183	33193

$$Q = \int \cos(\|x\|_2) \mathcal{N}(x : 0, I) dx$$

TABLE: True Value of Integral=-0.543583844.

Method	Q_{approx}	%err	min(w)	$\sum w_i $	N
<i>UT</i>	-0.6111	12.4130	0.0714	1	13
<i>HCKF - 5</i>	-0.4635]	14.7285	-0.0156	1.3750	73
<i>CUT4 - G</i>	-0.5492	1.0370	0.0039	1	76
<i>CUT6 - G</i>	-0.5419	0.3013	8.2885e-004	1	137
<i>CUT8 - G</i>	-0.5430	0.0995	7.8492e-005	1	745
<i>GH3</i>	-0.5162	5.0418	2.1433e-005	1	729
<i>GH4</i>	-0.5457	0.3918	9.3219e-009	1	4096
<i>GH5</i>	-0.5435	0.0229	2.0353e-012	1	15625
<i>GH6</i>	-0.5436	0.0011	2.7871e-016	1	46656
<i>GH7</i>	-0.5436	4.2494e-005	2.7162e-020	1	117649
<i>GH8</i>	-0.5436	1.4920e-006	2.0397e-024	1	262144
<i>GHS3</i>	-0.1910	64.8579	-2.5000	61	85
<i>GHS4</i>	-0.6023	10.7967	-30.0000	231	389
<i>GHS5</i>	-0.5370	1.2203	-13.3333	681	1433
<i>GHS6</i>	-0.5441	0.1026	-90.3333	1683	4541
<i>GHS7</i>	-0.5435	0.0068	-34.9444	3653	12841
<i>GHS8</i>	-0.5436	3.6928e-004	-199.3439	7183	33193

$$E[f(\mathbf{x})] = \int \mathcal{N}(\mathbf{x} : \mathbf{0}, \mathbf{P}_i) (\sqrt{1 + \mathbf{x}^T \mathbf{x}})^4 d\mathbf{x} \quad (1)$$

$$P_1 = \begin{bmatrix} 114.2595 & 90.1397 & 8.9751 \\ 90.1397 & 92.2504 & 29.1237 \\ 8.9751 & 29.1237 & 84.0908 \end{bmatrix}, \quad P_2 = 100I_{(10 \times 10)} \quad (2)$$

TABLE: GH vs CUT4: % rel. error and no. of points

method	n_1	ϵ_1 % error	n_2	ϵ_2 % error
UT	7	51.55	21	8.32
MC	1000	21.84	1000	4.41
MC	10000	3.59	10000	0.35
MC	100000	0.64	100000	0.0027
GH2	8	52.36	1024	16.39
GH3	27	$4.89e - 014$	59049	$7.23e - 012$
CUT4	14	0	1044	$6.72e - 012$

$$E[f(\mathbf{x})] = \int \mathcal{N}(\mathbf{x} : \mathbf{0}, \mathbf{P}_i) (\sqrt{1 + \mathbf{x}^T \mathbf{x}})^6 d\mathbf{x} \quad (3)$$

$$P_3 = 100I_{(4 \times 4)} \quad P_4 = 100I_{(9 \times 9)} \quad (4)$$

TABLE: GH vs CUT6: % rel. error and no. of points

method	n_3	ϵ_3 % error	n_4	ϵ_4 % error
UT	9	47.8	19	30.02
MC	1000	11.46	1000	7.65
MC	10000	2.09	10000	2.3
MC	100000	0.53	100000	0.058
GH3	81	12.45	19683	4.18
GH4	256	$2.31e - 013$	262144	$1.37e - 009$
CUT6	49	$6.49e - 013$	1203	$6.26e - 009$

$$E[f(\mathbf{x})] = \int \mathcal{N}(\mathbf{x} : \mathbf{0}, \mathbf{P}_i) (\sqrt{1 + \mathbf{x}^T \mathbf{x}})^8 d\mathbf{x} \quad (5)$$

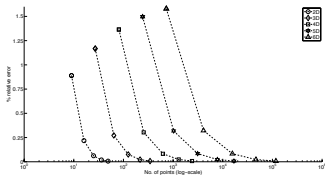
$$P_5 = 100I_{(5 \times 5)} \quad P_6 = 100I_{(6 \times 6)} \quad (6)$$

TABLE: GH vs CUT8: % rel. error and no. of points

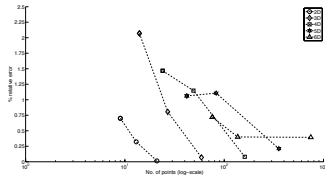
method	n_5	ϵ_5 % error	n_6	ϵ_6 % error
UT	11	68.74	13	64.19
MC	1000	19.514	1000	10.70
MC	10000	5.59	10000	5.17
MC	100000	0.43	100000	0.52
GH4	1024	3.45	4096	2.49
GH5	3125	$4.73e - 012$	15625	$9.29e - 012$
CUT8	355	$7.52e - 012$	745	$6.63e - 012$

NUMERICAL EXPERIMENTS

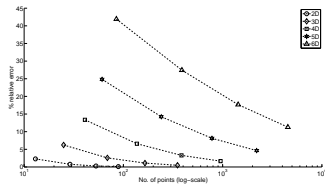
EXAMPLE: $E[(\sqrt{1+\mathbf{x}^T\mathbf{x}})^\alpha] = \int (\sqrt{1+\mathbf{x}^T\mathbf{x}})^\alpha \mathcal{N}(\mathbf{x}; \mathbf{0}, \mathbf{0.11}) d\mathbf{x}$



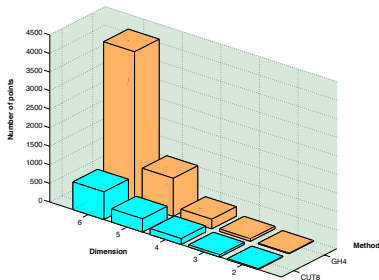
(a) Gauss-Hermite Convergence



(b) CUT Convergence



(c) Smolyak Scheme Convergence

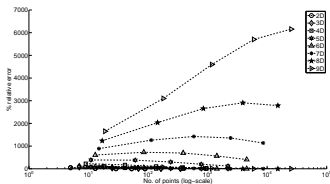


(d) Number of points required to achieve 0.5% Rel. error

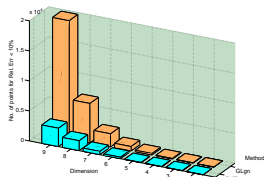
NUMERICAL EXPERIMENTS

NON-POLYNOMIAL FUNCTION

$$E[(\sqrt{1 + \mathbf{x}^T \mathbf{x}})^{-3}] = \frac{1}{2^N} \int_{-1}^1 (\sqrt{1 + \mathbf{x}^T \mathbf{x}})^{-3} d\mathbf{x}$$



(e) Smolyak Scheme Convergence



(f) Points required to achieve $\leq 10\%$ Relative error

- Longitudinal Dynamics Model:

$$\dot{\mathbf{x}} = \mathbf{A}\mathbf{x} + \mathbf{B}\delta, \quad \delta = -\mathbf{K}\mathbf{x}$$

$$\mathbf{x} = \begin{bmatrix} u_h \\ q_h \\ \theta_h \\ y \end{bmatrix}, \quad \mathbf{A} = \begin{bmatrix} p_1 & p_2 & -g & 0 \\ p_3 & p_4 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 1 & 0 & 0 & 0 \end{bmatrix}, \quad \mathbf{B} = \begin{bmatrix} p_5 \\ p_6 \\ 0 \\ 0 \end{bmatrix}$$

- Initial Conditions & Controller Gain:

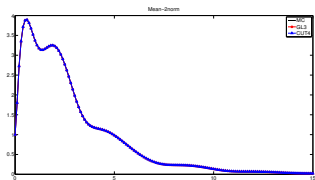
$$\mathbf{x}_0 = [0.7929, -0.0466, -0.1871, 0.5780]^T$$

$$\mathbf{K} = [1.9890, -0.2560, -0.7589, 1.0]$$

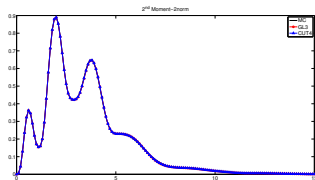
- Random Parameters: $\mathbf{p}_{lbd} = [-0.0488, 0.0013, 0.126, -3.3535]$
and $\mathbf{p}_{ubd} = [-0.0026, 0.0247, 2.394, -0.1765]$.

TABLE: 2-norm % Rel. Error

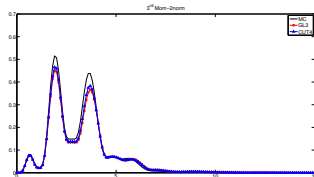
	GLgn3	CUT4-U	GLgn4	CUT6-U	GLgn5	CUT8-U
M_1	0.0176	0.0171	0.0161	0.0160	0.0160	0.0160
M_2	0.1150	0.0216	0.2338	0.2741	0.2576	0.2599
M_3	12.8793	9.9926	1.7471	0.4916	0.9488	0.9122
N	81	24	256	65	625	161



(g) 2-norm of Means



(h) 2-norm of 2nd order Moments

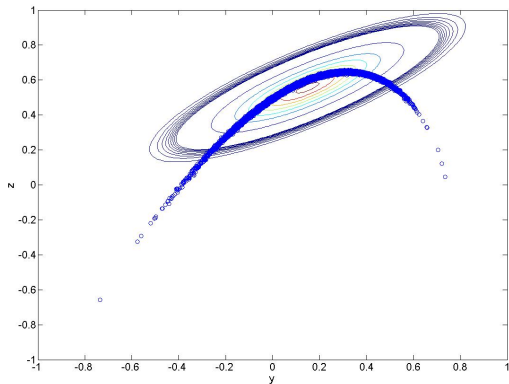


(i) 2-norm of 3rd order Moments

Figure: 2-norm of the Moments vs time

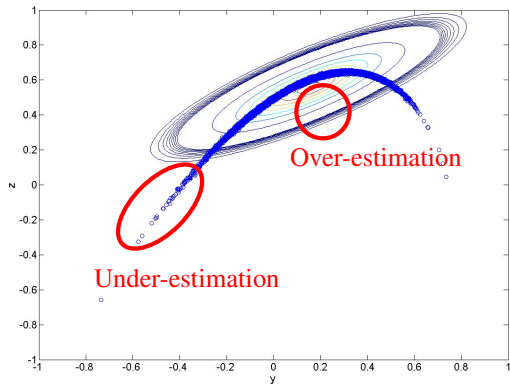
RECONSTRUCTING A PDF

MOTIVATION



RECONSTRUCTING A PDF

MOTIVATION



- Moments only provide indirect information about the shape of the pdf.
- Need to construct the pdf, preferably expressed by an analytical expression.
- **Problem Statement:** Given a set of moments, find the best pdf that can represent these moments.

PRINCIPLE OF MAXIMUM ENTROPY

$$\max_{p(x)} - \int p(x) \ln(p(x)) dx$$

s.t

$$\int x p(x) dx = M_1$$

$$\int x^2 p(x) dx = M_2$$

...

$$\int x^m p(x) dx = M_m$$

Using Lagrange Multipliers,

$$- \int p(x) \ln(p(x)) dx + \sum_{i=1}^m \lambda_i \left(\int x^i p(x) dx - M_i \right)$$

By calculus of variation, the optimal pdf is given analytically as

$$p(x) = \exp\left(\sum_{i=1}^m \lambda_i x^i\right)$$

- **Convex Optimization**
- Can be solved by Gradient search methods.
- Has to be numerically preconditioned as there is *exp(polynomial)*.

$$\int x \exp\left(\sum_{i=1}^m \lambda_i x^i\right) dx = M_1$$

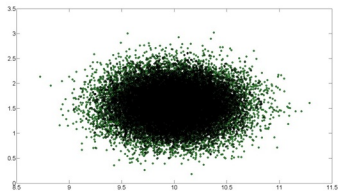
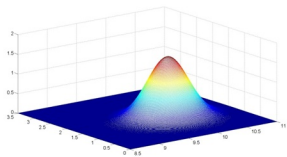
$$\int x^2 \exp\left(\sum_{i=1}^m \lambda_i x^i\right) dx = M_2$$

...

$$\int x^m \exp\left(\sum_{i=1}^m \lambda_i x^i\right) dx = M_m$$

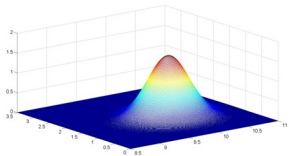
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES



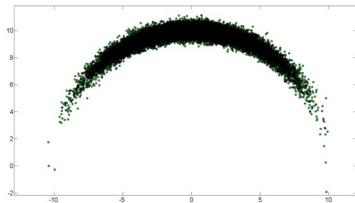
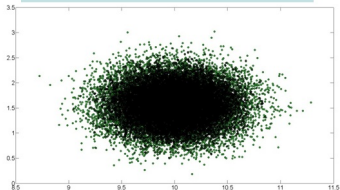
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES



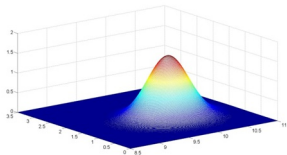
$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} r \cos \theta \\ r \sin \theta \end{bmatrix}$$

$$E \begin{bmatrix} x \\ y \end{bmatrix} = \int \begin{bmatrix} r \cos \theta \\ r \sin \theta \end{bmatrix} N \left(\begin{bmatrix} r \\ \theta \end{bmatrix}; \begin{bmatrix} \mu_r \\ \mu_\theta \end{bmatrix}, \Sigma \right)$$



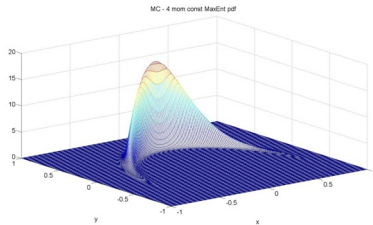
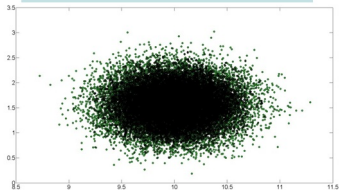
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

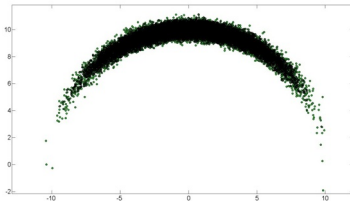


$$\begin{bmatrix} x \\ y \end{bmatrix} = \begin{bmatrix} r \cos \theta \\ r \sin \theta \end{bmatrix}$$

$$E \begin{bmatrix} x \\ y \end{bmatrix} = \int \begin{bmatrix} r \cos \theta \\ r \sin \theta \end{bmatrix} N(\begin{bmatrix} r \\ \theta \end{bmatrix}; \begin{bmatrix} \mu_r \\ \mu_\theta \end{bmatrix}, \Sigma)$$



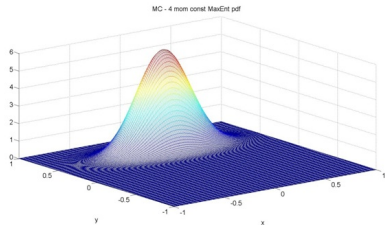
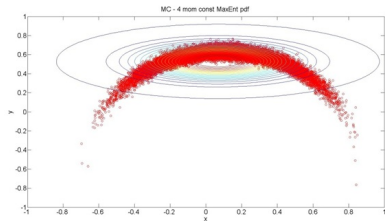
$$M_{(a,b)} = E[x^a y^b]$$
$$\forall a + b = d, \quad d = \{1, 2, \dots\}$$



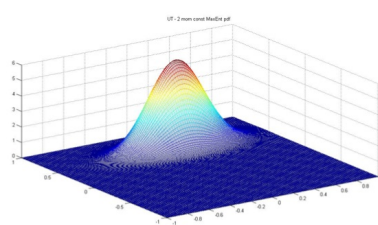
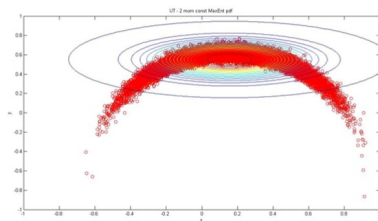
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 2nd order



Monte Carlo: 30000 samples

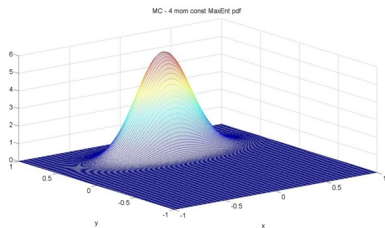
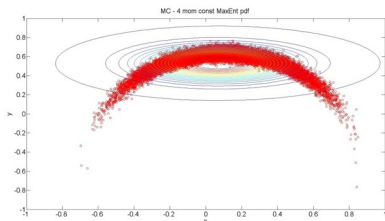


Unscented Transform:
5 points

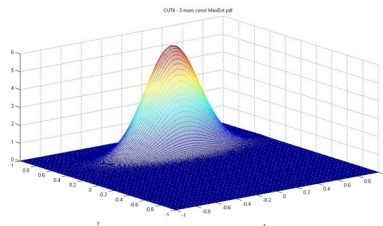
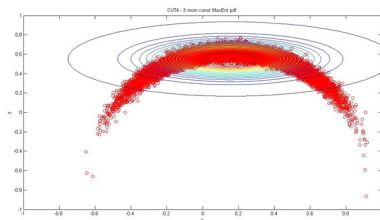
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 2nd order



Monte Carlo: 30000 samples



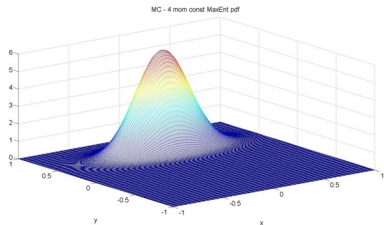
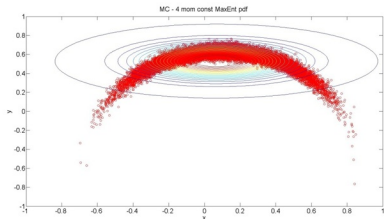
CUT4:
9 points



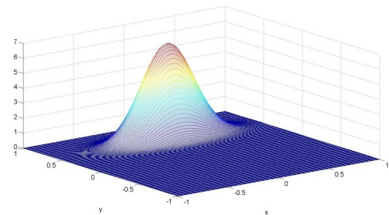
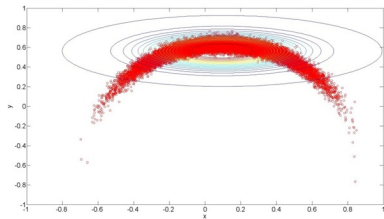
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 2nd order



Monte Carlo: 30000 samples



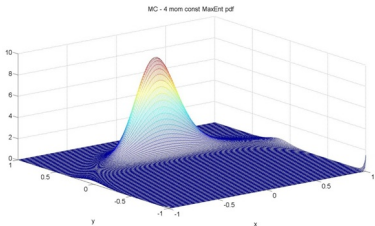
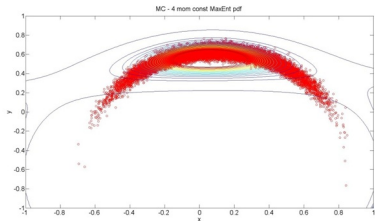
CUT8:
16 points



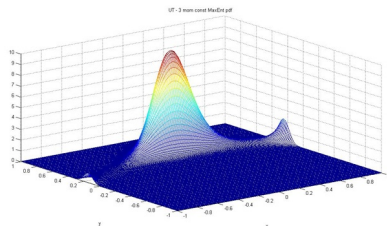
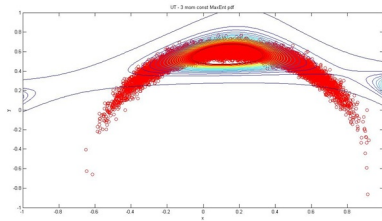
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 3rd order



Monte Carlo: 30000 samples

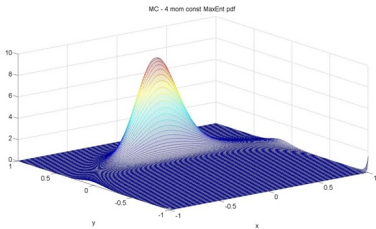
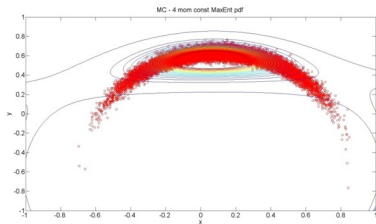


Unscented Transform:
5 points

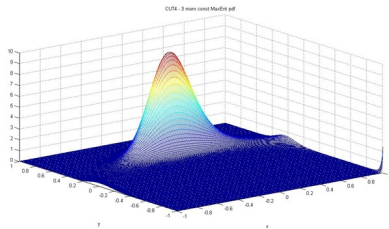
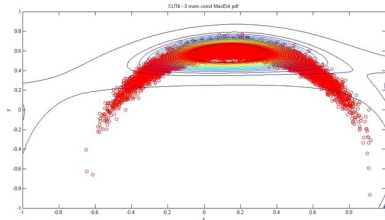
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 3rd order



Monte Carlo: 30000 samples

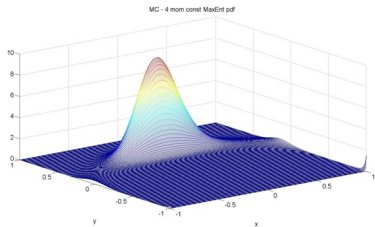
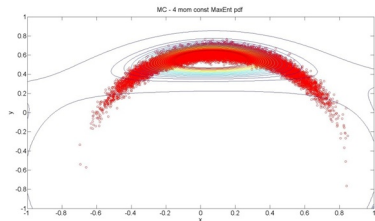


CUT4:
9 points

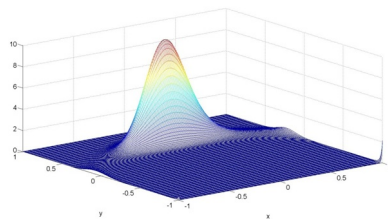
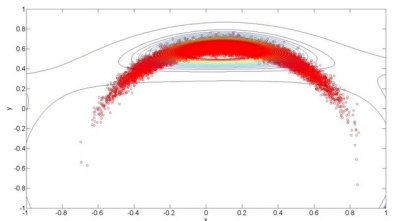
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 3rd order



Monte Carlo: 30000 samples

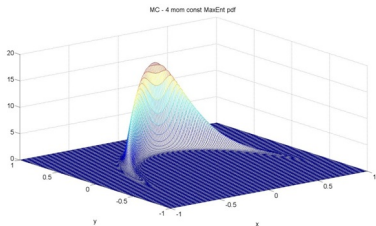
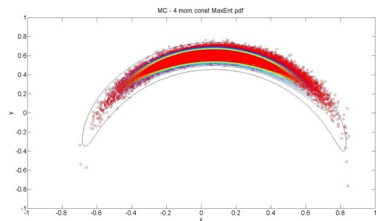


CUT8:
16 points

UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 4th order



Monte Carlo: 30000 samples

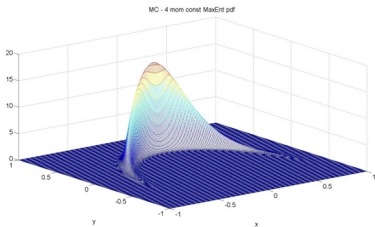
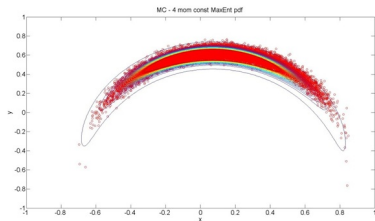
- Unscented Transform is only 3rd moment accurate
- Error in higher order moments
- Hence the pdf construction algorithm does not converge

Unscented Transform:
5 points

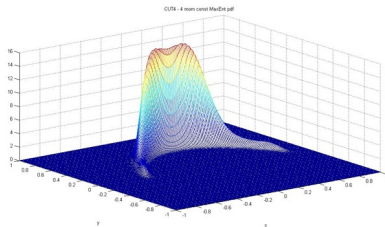
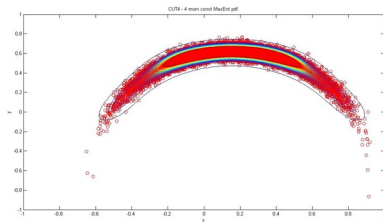
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 4th order



Monte Carlo: 30000 samples



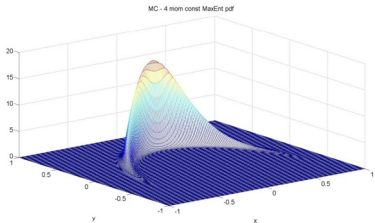
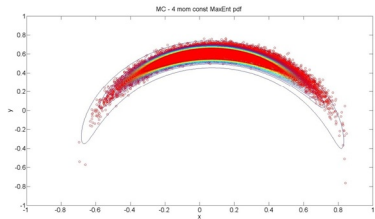
CUT4:
9 points



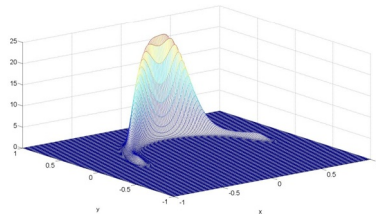
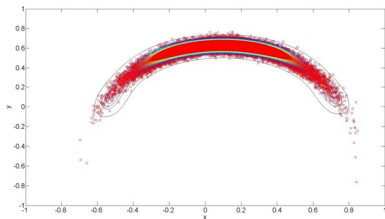
UNCERTAINTY TRANSFORMATION

PDF TRANSFORMATION UNDER POLAR TO CARTESIAN COORDINATES

Using moments upto 4th order



Monte Carlo: 30000 samples



CUT8:
16 points

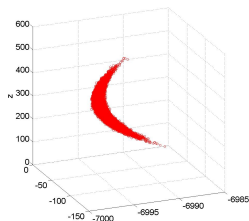
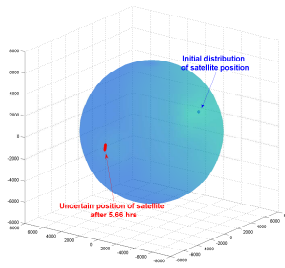
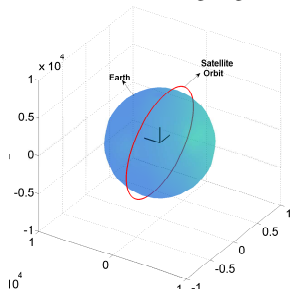
EXAMPLE PDF RECONSTRUCTION

TWO BODY PROBLEM

3D, there are

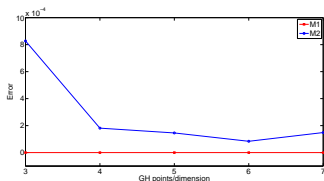
- 3 : 1st order moments
- 6 : 2nd order moments
- 10 : 3rd order moments
- 15 : 4th order moments
- A total of 34 lagrange multipliers to solve

- Reconstructing the pdf of Satellite position in full 3D.
- For visualization, this pdf is marginalized into 2D
- pdf contours compared against 200,000 MC runs

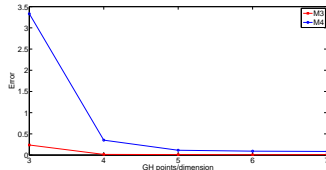


TWO BODY PROBLEM

MOMENTS EVALUATION



(a) All 1st and 2nd order moments



(b) All 3rd and 4th order moments

Figure: Error compared to GH8 (8 points in each dimension)

$$\ddot{x} = -\frac{\mu x}{r^3} + J_{2x} + a_{Dx}, \quad J_{2x} = -1.5J\left(\frac{\mu}{r^2}\right)\left(\frac{R_e}{r}\right)^2\left(1-5\frac{z^2}{r^2}\right)\frac{x}{r}$$

$$\mathbf{x}(0) \sim \mathcal{N}(\boldsymbol{\mu}_0, \mathbf{P}_0) \text{ where}$$

$$\ddot{y} = -\frac{\mu y}{r^3} + J_{2y} + a_{Dy}, \quad J_{2y} = -1.5J\left(\frac{\mu}{r^2}\right)\left(\frac{R_e}{r}\right)^2\left(1-5\frac{z^2}{r^2}\right)\frac{y}{r}$$

$$\boldsymbol{\mu}_0 = [7000, 0, 0, 0, -1.0374090357, 7.4771288355]^T$$

$$\ddot{z} = -\frac{\mu z}{r^3} + J_{2z} + a_{Dz}, \quad J_{2z} = -1.5J\left(\frac{\mu}{r^2}\right)\left(\frac{R_e}{r}\right)^2\left(3-5\frac{z^2}{r^2}\right)\frac{z}{r}$$

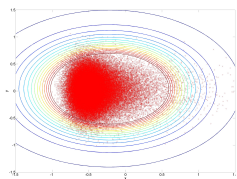
$$\mathbf{P}_0 = \text{diag}[0.01, 0.01, 0.01, 0.000001, 0.000001, 0.000001]$$

TABLE: RMSE in UT-CUT-GH5 (cartesian coordinates)

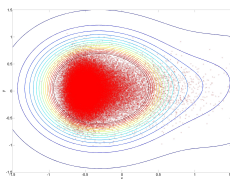
RMSE in	UT	CUT4	CUT6	CUT8	GH5	MC 100,000
e_1	1.18099856e-6	8.293251541e-10	4.2115520e-10	3.606078697e-10	2.809932915e-10	0.0330
e_2	0.186046892	0.0007910991	0.0011943952	0.0001853985	0.0001455770	0.8689
e_3	6.5478634011	0.2308841835	0.0107398551	0.009191179	0.012293992	4.6141
e_4	35.112930371	3.2570295399	0.205353106	0.0894419280	0.1143631243	4.6670

TWO BODY PROBLEM

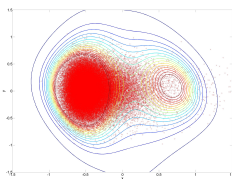
RECONSTRUCTING THE POSITION PDF WITH CUT4



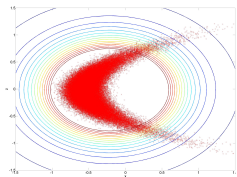
(a) (x,y) : upto 2nd order



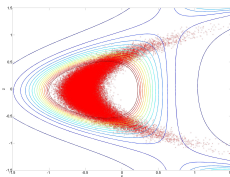
(b) (x,y) : upto 3rd order



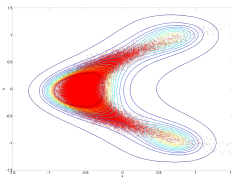
(c) (x,y) : upto 4th order



(d) (x,z) : upto 2nd order



(e) (x,z) : upto 3rd order



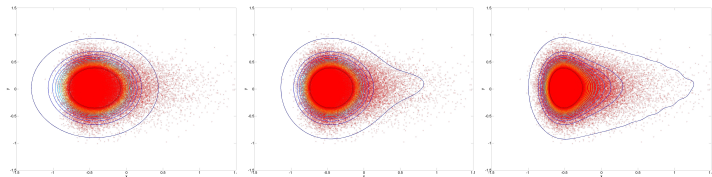
(f) (x,z) : upto 4th order

Figure: *CUT4: Marginalized pdf reconstruction using all 3D moments³*

³N. Adurthi and P. Singla, "A Conjugate Unscented Transformation Based Approach for Accurate Conjunction Analysis," *AIAA Journal of Guidance, Control & Dynamics*, 2015.

TWO BODY PROBLEM

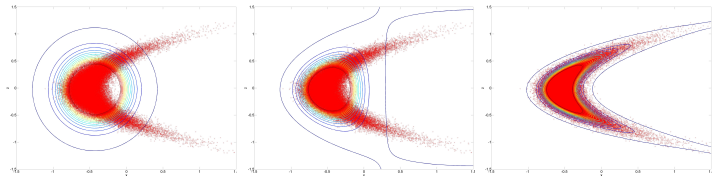
RECONSTRUCTING THE POSITION PDF WITH CUT6



(a) (x,y) : upto 2nd order

(b) (x,y) : upto 3rd order

(c) (x,y) : upto 4th order



(d) (x,z) : upto 2nd order

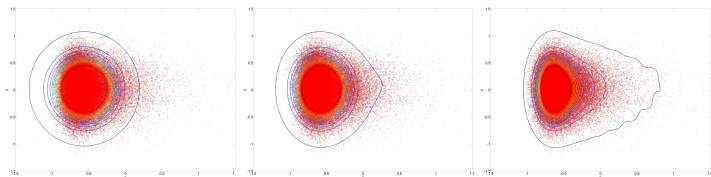
(e) (x,z) : upto 3rd order

(f) (x,z) : upto 4th order

Figure: *CUT6: Marginalized pdf reconstruction using all 3D moments*

TWO BODY PROBLEM

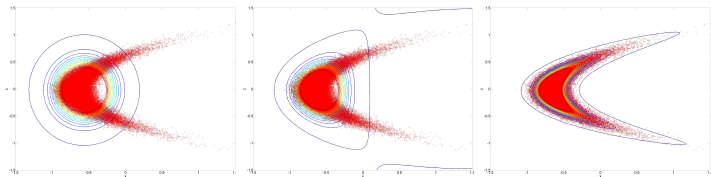
RECONSTRUCTING THE POSITION PDF WITH CUTS



(a) (x,y) : upto 2nd order

(b) (x,y) : upto 3rd order

(c) (x,y) : upto 4th order



(d) (x,z) : upto 2nd order

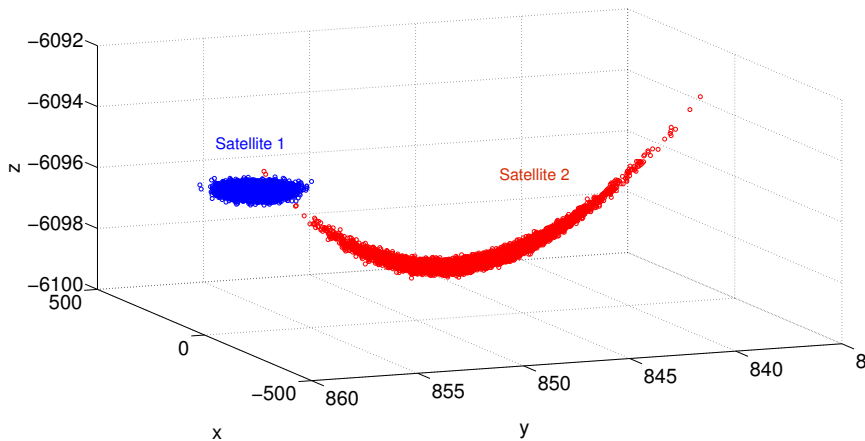
(e) (x,z) : upto 3rd order

(f) (x,z) : upto 4th order

Figure: *CUT8: Marginalized pdf reconstruction using all 3D moments*

TWO BODY PROBLEM

PROBABILITY OF COLLISION



TWO BODY PROBLEM

PROBABILITY OF COLLISION

Miss distance

$$\mathbf{d} = \mathbf{x} - \mathbf{y}$$

position of Satellite 1 (pointing to \mathbf{x})
position of Satellite 2 (pointing to \mathbf{y})

Probability that the objects are within a region Ω

sphere of radius R : $P(\|\mathbf{d}\| < R)$

cube of half side length R : $P(\|\mathbf{d}\|_{max} < R)$

Monte Carlo simulations

$$\frac{\text{No. of samples within } \Omega}{\text{Total no. of samples}}$$

Probability Density Approach

$$\int_{\Omega} p_d(\mathbf{x}) d\mathbf{x}$$

If x and y are Gaussian random variables

$$x \sim N(x; \mu_x, P_x)$$

$$y \sim N(y; \mu_y, P_y)$$

then $d \sim N(d; \mu_d, P_d)$

$$\mu_d = \mu_x - \mu_y$$

$$P_d = P_x + P_y$$

TWO BODY PROBLEM

PROBABILITY OF COLLISION

$$\rho = x - y$$

Moments of ρ can be computed analytically, given the moments of x and y

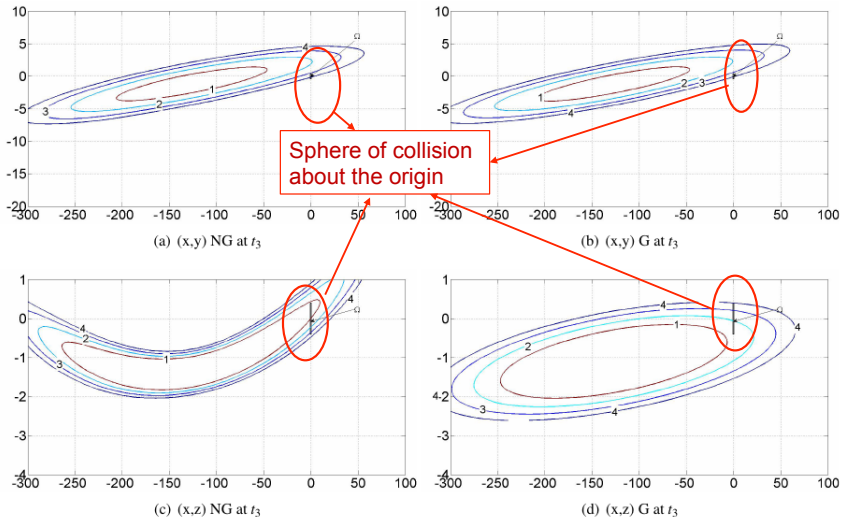
First Order	$E[\rho_1]$	$E[\rho_2]$	$E[\rho_3]$			
Second Order	$E[\rho_1^2]$	$E[\rho_2^2]$	$E[\rho_3^2]$	$E[\rho_1\rho_2]$	$E[\rho_2\rho_3]$	$E[\rho_1\rho_3]$
Third Order	$E[\rho_1^3]$	$E[\rho_2^3]$	$E[\rho_3^3]$	$E[\rho_1^2\rho_2]$	$E[\rho_2^2\rho_3]$	$E[\rho_1^2\rho_3]$
	$E[\rho_1\rho_2^2]$	$E[\rho_2\rho_3^2]$	$E[\rho_1\rho_3^2]$	$E[\rho_1\rho_2\rho_3]$		
Fourth Order	$E[\rho_1^4]$	$E[\rho_2^4]$	$E[\rho_3^4]$	$E[\rho_1^2\rho_2^2]$	$E[\rho_2^2\rho_3^2]$	$E[\rho_1^2\rho_3^2]$
	$E[\rho_1^2\rho_2\rho_3]$	$E[\rho_1\rho_2^2\rho_3]$	$E[\rho_1\rho_2\rho_3^2]$	$E[\rho_1^3\rho_2]$	$E[\rho_2^3\rho_3]$	$E[\rho_1^3\rho_3]$
	$E[\rho_1\rho_2^3]$	$E[\rho_2\rho_3^3]$	$E[\rho_1\rho_3^3]$			

Table 13. Case 2: RMSE in Computing Moments for Miss-Distance for Different Algorithms as Compared to GH7.

RMSE	GH4	GH5	CUT6	CUT8
e_1	4.5503e-011	1.858e-009	2.3286e-009	7.2916e-010
e_2	5.043e-008	3.8458e-007	8.2925e-006	7.8087e-008
e_3	1.5397e-005	6.5314e-005	0.0033037	1.327e-005
e_4	0.35904	0.010302	1.0176	0.0098918
N	4096	15625	137	745

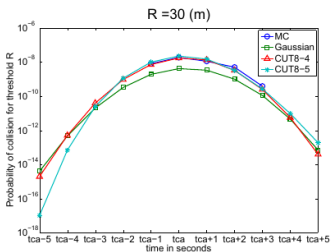
TWO BODY PROBLEM

PROBABILITY OF COLLISION

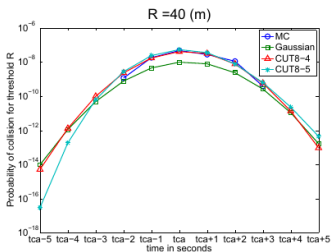


TWO BODY PROBLEM

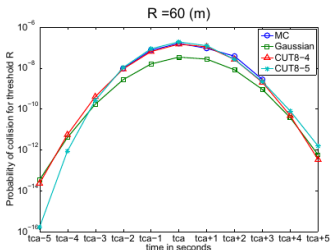
PROBABILITY OF COLLISION



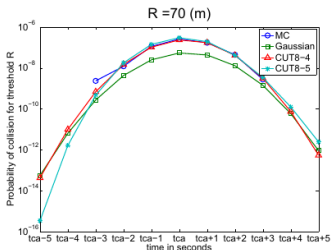
(a) $R = 30m$



(b) $R = 40m$



(c) $R = 60m$

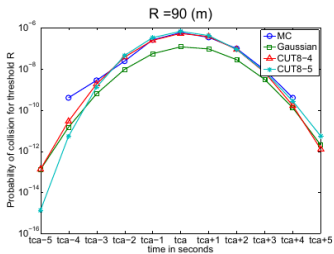


(d) $R = 70m$

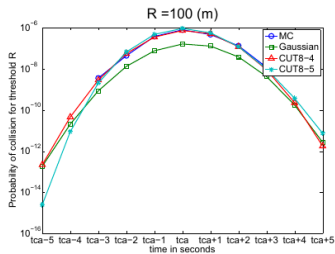
Figure: 10 Million MC Runs vs. 1490 CUT Runs

TWO BODY PROBLEM

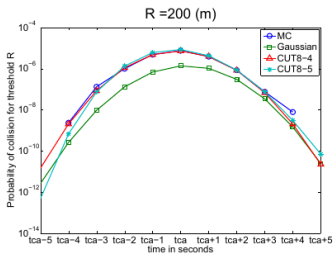
PROBABILITY OF COLLISION



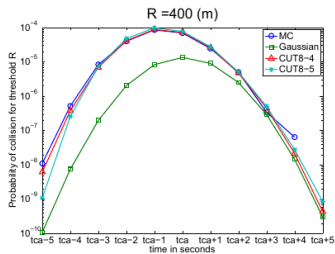
(a) $R = 90m$



(b) $R = 100m$



(c) $R = 200m$



(d) $R = 400m$

Figure: 10 Million MC Runs vs. 1490 CUT Runs

NUMERICAL INTEGRATION

$$E[f(\mathbf{x})] = \int f(\mathbf{x})p(\mathbf{x}) d\mathbf{x} \approx \sum_{i=1}^N w_i f(\mathbf{x}_i)$$

Monte Carlo Simulations

- Random points $\mathbf{x}_i \sim p(\mathbf{x})$
- Slow convergence : of order $\frac{1}{\sqrt{N}}$
- Large number of simulation are required

Gaussian Quadratures

- Fixed weights and points (roots of special polynomials)
- Faster convergence
- Tensor product of 1D points
- Exponential growth of points with dimension

Unscented Transform

- For n-Dimensions: just $2n + 1$ points required for 3^{rd} degree polynomials
- $2n + 1 \ll 2^n$ (Gaussian Quadratures)
- Error when used for higher degree polynomials

Smolyak Sparse Grid Quadrature

- Avoids tensor product by special sparse product of points
- Can contain negative weights

Non-product cubature rules- CUT

- Construct the points directly in the dimension required
- Avoid taking product of lower dimensional rules like Tensor Product and Sparse product
- Often results in a small fraction of point compared to Gaussian Quadratures and Smolyak quadrature